

1 **The role of CNC surface modification on the**  
2 **structural, thermal and electrical properties of**  
3 **poly(vinylidene fluoride) nanocomposites**

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22 **Abstract**

23 This work reports on the effect of cellulose nanocrystal (CNC) surface charge in the  
24 structure and dielectric properties of poly (vinylidene fluoride) (PVDF)  
25 nanocomposites. CNCs extracted through sulfuric acid hydrolysis were modified using  
26 sodium hydroxide and cationization treatments to yield CNCs with zeta-potential values  
27 of  $-26.1 \pm 3.7$  and  $-4.4 \pm 0.3$  mV in comparison with the original highly-negative  $-45.2$   
28  $\pm 1.1$  mV. Nanocomposites with a concentration up to 25 wt% CNC have been obtained  
29 through doctor-blade casting followed by room temperature drying. The induced  
30 changes on the morphology, structure, thermal and dielectric response depending on the  
31 CNC concentration and surface-charge are investigated. CNC incorporation allows  
32 obtaining PVDF comprising 100 % of  $\gamma$ -phase. Further, an increase of the real  
33 dielectric constant  $\epsilon'$ , dielectric loss  $\tan \delta$  and ac conductivity values are observed in the  
34 nanocomposites by increasing CNC content. More importantly, these values are further  
35 increased upon CNC surface-modification, suggesting the relevance of the interfacial  
36 contributions to the dielectric response and that the sulfate half-ester removal to yield –  
37 OH groups is able to increase the amount of accumulated charges at the PVDF-CNC  
38 interfaces.

39

40

41 **Keywords:** A: Polymer-matrix composites (PMCs); B: Electrical properties; D:  
42 Infrared (IR) spectroscopy; D: X-ray diffraction (XRD); cellulose nanocrystals.

## 43 **1. Introduction**

44 Poly (vinylidene fluoride) (PVDF) is a semicrystalline thermoplastic with relevant  
45 technological electroactive properties for sensor and actuator applications. Its  
46 ferroelectric, pyroelectric and piezoelectric properties strongly depend on the type of  
47 crystalline polymorph present in the material, which comprises  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $\delta$  or  $\epsilon$  phases [1-  
48 3]. Among them, the  $\beta$ -phase is the one with the largest net dipole moment and  
49 piezoelectric response [2]. As melt-processing technologies typically result in the  
50 formation of the non-polar  $\alpha$ -phase, many efforts has been carried out in order to  
51 promote the formation of  $\beta$ -phase PVDF [2], including poling [4], thermal treatment [5],  
52 stretching [6] or nanocomposite development [7, 8]. The other relevant electroactive  
53 phase it the  $\gamma$  phase. This phase shows a piezoelectric response of -7 pC/N and can be  
54 obtained by reinforcing PVDF with clays and other fillers [9]. Interestingly, this phase  
55 has been gathering increasing attention with applications in the areas of optical sensors  
56 and actuators [9, 10].

57 As particles can be directly incorporated during the fabrication process,  
58 nanocomposite development can be seen as one of the preferred approach due to its  
59 simplicity. Moreover, the presence of nanofillers typically enhances other  
60 technologically relevant macroscopic properties of the hosting matrix such as electrical  
61 [11], mechanical [12], thermal [13], optical [14], or barrier properties [15].

62 The use of inorganic nanofillers (carbon nanotubes, barium titanate or cobalt ferrite,  
63 among others) to nucleate the electroactive phases of PVDF has been deeply  
64 investigated in the past [16-18]. However, the use of organic nanoparticles remains still  
65 in its infancy. In this regard, cellulose nanocrystals (CNCs) could be considered as one  
66 of the most promising fillers due to their anisotropic character (large surface-area),  
67 renewability, cost-effectiveness, low-density, compostability, mechanical stability with a

68 high Young's modulus (130 GPa), and simple surface modification [19-21]. Although  
69 CNCs can be extracted from cellulosic sources upon controlled mechanical, chemical or  
70 enzymatic disintegration, sulfuric acid hydrolysis is the most commonly used method  
71 [22]. This approach yields CNC surfaces with negatively charged half-ester groups (-  
72 OSO<sub>3</sub><sup>-</sup>). Thanks to the fact that the surface chemistry of CNCs can be easily modified  
73 due to the many surface hydroxyl (-OH) groups, tailored functionalities can be  
74 incorporated. Additionally, the highly crystalline character of CNCs may help to  
75 enhance the inherent piezoelectric effect of wood, contributing to increase the  
76 overall piezoelectric behaviour of the resulting nanocomposite [23].

77 Till the date several studies have focused on the understanding of how the surface  
78 modification of CNCs alters the properties of resulting polymer nanocomposites. For  
79 instance, the ionic strength of aqueous CNC dispersions can be modified with  
80 surfactants such as cetyltrimethylammonium bromide, allowing their dispersion within  
81 solvent/matrices of decreasing polarity [24]. Lizundia et al. reported that the  
82 modification of CNC surface charge can lead to enhanced electrochemical performance  
83 of CNC/polypyrrole composites [25]. Acetylation was pursued to increase the  
84 interfacial adhesion of CNCs with the hosting poly(butylene succinate) matrix [26].  
85 Alanis et al. modified CNCs by means of plasma-surface modification and reported a  
86 significantly enhanced impact resistance of the hosting acrylonitrile butadiene styrene  
87 polymer matrix [27].

88 Till the date PVDF/cellulose nanocomposites have been studied for applications as  
89 varied as filtration [28], and self-powering electronic textiles [29]. It was found that the  
90 addition of microcrystalline cellulose (MCC) induces  $\beta$ -phase PVDF, negatively  
91 impacting the mechanical performance [30]. In the case of electrospun PVDF/cellulose  
92 nanofibers, the presence of cellulose barely affects the  $\beta$ -phase content and the total

93 crystallinity of PVDF, although the dielectric constant values markedly increased with  
94 cellulose content [31]. Recently, for PVDF/cellulose nanofibril composites it has been  
95 demonstrated the nucleation of the PVDF  $\gamma$ -phase, where the thermal and mechanical  
96 properties depend on the cellulose nanofibril concentration [32].

97 Taking into consideration the previous works carried out in the field of PVDF/CNC  
98 composites, it results critical to understand how CNCs having different surface charges  
99 can serve as heterogeneous nucleation sites for electroactive phases of PVDF.  
100 Therefore, CNCs being highly negative, slightly negative and neutral have been  
101 incorporated into PVDF at different concentrations and the resulting physico-chemical  
102 properties and polymer crystalline conformation of the nanocomposites has been  
103 studied. Finally, the dielectric properties have been also investigated.

104

## 105 **2. Materials and Methods**

### 106 *2.1. Starting materials*

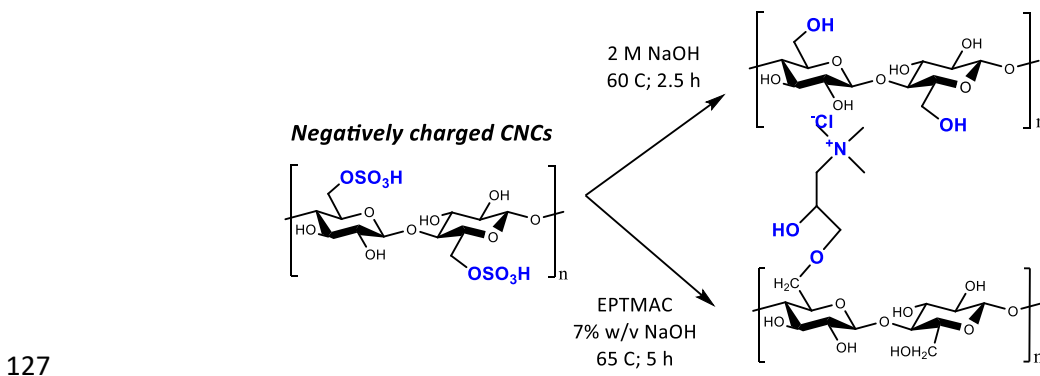
107 Microcrystalline cellulose with an average particle size of 20  $\mu\text{m}$  (310697-500G),  
108 sulphuric acid (95 - 97 %, 30743-1L) and dimethylformamide (DMF) have been  
109 supplied by Sigma Aldrich and used as received. Poly (vinylidene fluoride) (PVDF)  
110 with a number-average molecular weight of  $M_w = 570\text{-}600 \text{ kg}\cdot\text{mol}^{-1}$  was purchased  
111 from Solvay (Solef 6020).

112

### 113 *2.2. CNCs synthesis and CNC surface modification*

114 Cellulose nanocrystals (CNCs) are extracted from microcrystalline cellulose by  
115 sulfuric acid hydrolysis followed by sonication [22, 33]. 5 g of commercial  
116 microcrystalline cellulose were hydrolyzed in 100 mL of aqueous 64 % (w/w) sulphuric  
117 acid solution at 45  $^{\circ}\text{C}$  for 30 min under magnetic stirring at 500 rpm. The reaction was

118 stopped by adding 1 L of cold distilled water. The suspension was centrifuged at 5000  
 119 rpm for 10 min to remove the excess of acid. Colloidal cellulose was obtained via  
 120 sonication in a Vibracell Sonicator (Sonicsand Materials Inc., Danbury, CT) at 50%  
 121 output for 10 min. For further purification, the suspension was dialyzed during 7 days  
 122 using a Visking dialysis membrane with a molecular weight cut off of 12.000-14.000  
 123 Da (Medicell Membranes Ltd). An aqueous CNC dispersion with a pH of 2.3 and a  
 124 concentration of 1.5 % w/w was obtained. As sulfuric acid hydrolysis yields negatively  
 125 charged CNCs, further modification steps are required to decrease its negative character  
 126 (see Fig. 1).



128 **Fig. 1.** Water-dispersed CNCs underwent two different surface treatments to obtain surface modified  
 129 CNCs.

130

131 Due to the regioselectivity of the reactions, CNC surface modification is carried out  
 132 at the C6 position. Slightly negative CNCs were obtained upon the removal of the  
 133 surface anionic sulfate ester groups ( $-\text{OSO}_3^-$ ) by a 2 M NaOH solution at 60 °C [34].  
 134 After 2.5 h the reaction was quenched with 5-fold distilled water and the excess of  
 135 NaOH was removed by centrifugation as described above. Positive groups onto CNCs  
 136 were incorporated after the reaction of the C6 carbon atom with  
 137 epoxypropyltrimethylammonium chloride (EPTMAC) to yield CNCs with cationic  
 138 hydroxypropyltrimethylammonium chloride substituents [35]. Water dispersed CNCs

139 where exchanged into a 7% w/v NaOH solution. After 30 minutes at room temperature,  
140 10 mg of EPTMAC were added and it was allowed to react for 5 h at 65 °C. The  
141 reaction was also stopped by adding 5-fold distilled water followed by centrifugation.

142 In order to incorporate CNCs into PVDF, water-dispersed CNCs have been  
143 exchanged to DMF through centrifugation. Firstly, 5 mL of acetone are added to  
144 aqueous CNC dispersions before centrifugation at 5000 rpm for 10 min. The  
145 supernatants are poured off and the remaining CNCs are washed two times with acetone  
146 and three times with DMF using the same centrifuge parameters. Re-suspended  
147 solutions are submitted to sonication for 4 min after each step during the solvent  
148 exchange to avoid CNC aggregation. DMF-dispersed CNCs were stored at 4 °C.

149

### 150 *2.3. Nanocomposite preparation*

151 PVDF/CNC nanocomposite films were obtained by doctor-blade casting as reported  
152 previously [36]. After dissolving the PVDF into DMF, the required amount of CNCs  
153 was added to obtain 14 % (by weight) dispersions. After dispersion by magnetic stirring  
154 and sonication, the mixtures were deposited by the doctor blade technique onto a clean  
155 glass substrate allowing DMF to evaporate at 80 °C. Neat PVDF films were also  
156 prepared for comparison. Samples with an average thickness of  $40 \pm 10 \mu\text{m}$  were  
157 obtained by this method.

158

### 159 *2.4. Characterization*

160 Modified CNCs were observed under a Philips CM120 Biofilter transmission  
161 electron microscopy (TEM) with STEM module at an acceleration voltage of 120 kV. A  
162 droplet of aqueous CNC suspension ( $0.1 \text{ mg}\cdot\text{mL}^{-1}$ ) was negatively stained with 1%  
163 uranyl acetate ( $\text{UO}_2(\text{CH}_3\text{COO})_2$ ) for 1 min before analysis [33]. CNC surface charge

164 was determined by Zeta-potential measurements using a Malvern Zetasizer Nano-ZS  
165 (0.1 mg·mL<sup>-1</sup>). PVDF/CNC nanocomposites were observed with a scanning electron  
166 microscope (SEM, NanoSEM - FEI Nova 200 (FEG/SEM)) at an accelerating voltage  
167 of 15 kV. Before analysis, samples were coated with a gold layer by sputtering with a  
168 Polaron SC502 apparatus. Attenuated total reflectance Fourier transform infrared  
169 spectroscopy (ATR-FTIR) of PVDF/CNC nanocomposites was carried out in a Jasco  
170 FT/IR-4100 system in the range of 4000 - 600 cm<sup>-1</sup> with a resolution of 2 cm<sup>-1</sup>. Wide  
171 angle X-ray diffraction (WAXD) measurements were performed on a PANalytical  
172 Empyrean diffractometer in reflection mode using Cu K $\alpha$  radiation ( $\lambda = 1.5418 \text{ \AA}$ ) and  
173 operating at 45 kV and 40 mA. Thermal transitions of nanocomposites were studied  
174 with a Netzsch DSC 204 F1 Phoenix differential scanning calorimetry (DSC) under  
175 nitrogen flow in the range of 25-200 °C at a rate of 10 °C·min<sup>-1</sup> for both cooling and  
176 heating. All samples were measured in 40  $\mu$ L aluminium pans with perforated lids.

177 The dielectric response of the materials was obtained by measuring at room  
178 temperature the capacity (C) and dielectric losses ( $\tan \delta$ ) with a Quadtech 1920 LCR  
179 precision Meter in the 20 Hz - 1 MHz frequency range with an applied voltage of 0.5 V.  
180 5 mm diameter aluminum electrodes were vacuum evaporated onto both sides of each  
181 sample (2% error) to obtain samples with a parallel plate condenser configuration. The  
182 real part of the dielectric function ( $\epsilon'$ ) and the real part of the electrical conductivity ( $\sigma'$ )  
183 were obtained according to:

184 
$$\epsilon' = \frac{C \cdot d}{\epsilon_0 \cdot A} \quad (1)$$

185 
$$\tan \delta = \frac{\epsilon''}{\epsilon'} \quad (2)$$

186 
$$\sigma' = \epsilon_0 \omega \epsilon'' \quad (3)$$

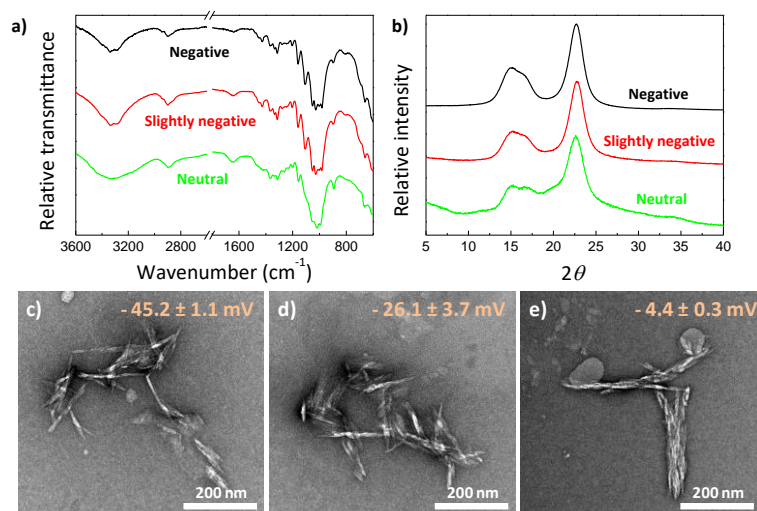


187 where  $A$  indicates the plate area,  $d$  is a plate distance,  $\epsilon_0$  ( $8.85 \times 10^{-12} \text{ F} \cdot \text{m}^{-1}$ ) is the  
188 permittivity of free space,  $\epsilon'$  and  $\epsilon''$  are the real and imaginary dielectric constant  
189 respectively and  $\omega = 2\pi\nu$  is the angular frequency.

### 190 **3. Results and discussion**

#### 191 *3.1. CNC surface modification*

192 To study the effect of CNC surface charge on the resulting structural and dielectric  
193 properties of PVDF/CNC nanocomposites, CNCs having three different surface charges  
194 have been obtained upon surface modification as shown in Fig. 1. Fourier transform  
195 infrared spectroscopy (FTIR) and wide-angle X-ray diffraction (WAXD) measurements  
196 were conducted to confirm the successful modification of CNCs. Fig. 2a shows the  
197 FTIR spectra of surface modified CNCs. All three samples present the characteristic  
198 peaks of cellulose, with the broad  $3650\text{--}3200 \text{ cm}^{-1}$  band due to the O-H stretching, the  
199  $2902 \text{ cm}^{-1}$  corresponding to the asymmetric C-H stretching and further bands at  $1337$   
200  $\text{cm}^{-1}$ ,  $1160 \text{ cm}^{-1}$  and  $897 \text{ cm}^{-1}$  due to C-O-H bending, C-O-C bending and to C-O-C  
201 asymmetric stretching respectively [21, 33]. As a result of the NaOH treatment, treated  
202 CNCs present a decreased intensity of the  $1033 \text{ cm}^{-1}$  band, indicating the partial  
203 removal of  $-\text{SO}_3$  groups from the CNC surfaces [34]. Moreover, two new peaks at  $1640$   
204  $\text{cm}^{-1}$  and  $1480 \text{ cm}^{-1}$  arise for CNCs modified with EPTMAC. Such bands are indicative  
205 of the adsorbed water as a result of cationization-induced hydrophilization and of the C-  
206 N vibration of cationic hydroxypropyltrimethylammonium chloride substituents  
207 respectively [35].



208

209 **Fig. 2.** Characterization of modified CNCs. a) FTIR spectra; b) WAXD patterns and TEM images of c)  
 210 negative CNCs, d) slightly negative CNCs and e) nearly neutral CNCs. Measured zeta-potential is shown  
 211 as an inset on the top of TEM images.

212

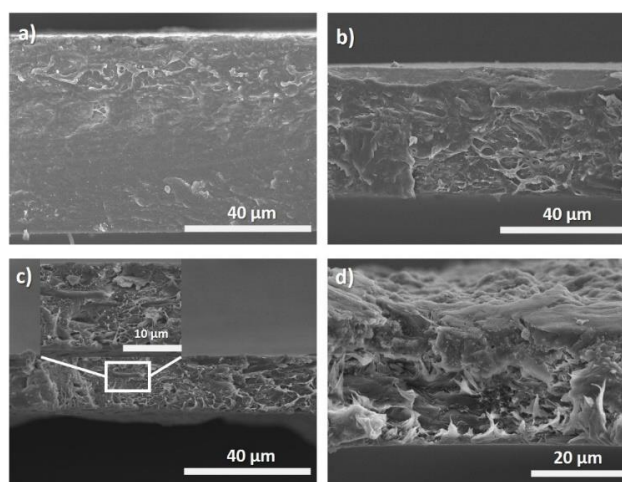
213 Due to the modifications carried out, the initially highly negative CNCs, with a zeta-  
 214 potential of  $-45.2 \pm 1.1$  mV leads to slightly negative ( $-26.1 \pm 3.7$  mV) and nearly  
 215 neutral ( $-4.4 \pm 0.3$  mV) CNCs after NaOH treatment and NaOH/ EPTMAC treatment.  
 216 These results suggest that NaOH does not successfully remove all the negatively-  
 217 charged anionic sulfate ester groups ( $-\text{OSO}_3^-$ ) from CNC surfaces as still the overall  
 218 charge of CNCs remains negative. As a result of that, EPTMAC treatment serves to  
 219 introduce positively-charged moieties onto CNC surfaces, which may counteract the  
 220 charge of the remaining negative  $-\text{OSO}_3^-$  groups to yield neutral CNCs. Despite the  
 221 surface modification of the CNCs, their crystalline structure and morphological features  
 222 remain barely unchanged as indicated by the WAXD patterns in Fig. 2b and TEM  
 223 micrographs in Fig. 2c-e respectively. Indeed, for all three samples WAXD patterns  
 224 display the characteristic diffraction peaks of cellulose I at  $2\theta = 14.9^\circ, 16.5^\circ, 22.7^\circ$  and  
 225  $34.4^\circ$ , which correspond to  $(1-10)$ ,  $(101)$ ,  $(200)$  and  $(004)$  planes respectively [37, 38].  
 226 Additionally, CNCs present a length of  $160 \pm 35$  nm (statistics based on 30 particle

227 counts) independently of the surface modification, indicating that the initial morphology  
228 of CNCs (those extracted upon sulphuric acid hydrolysis) is kept after NaOH and  
229 EPTMAC treatment.

230

### 231 *3.2. Morphology, physicochemical conformation and crystalline structure of the* 232 *nanocomposites*

233 The morphological changes of the PVDF/CNC nanocomposites induced by the  
234 presence of surface-modified CNCs have been investigated by field-emission scanning  
235 electron microscopy (FE-SEM). Accordingly, Fig. 2a-c display the cross-section of  
236 cryogenically fractured PVDF/CNC nanocomposites for different negatively charged  
237 CNC concentrations (0, 5 and 25 %). For neat PVDF (Fig. 2a), a dense and a relatively  
238 smooth surface is observed. Surface roughness increases with CNC concentration as  
239 shown in Fig. 2b-c, where an homogeneous distribution of CNCs with no aggregates  
240 along the cross-section is observed. Fig. 2d suggests that CNC surface charge does not  
241 affect the morphology of PVDF/CNC nanocomposites as no relevant changes are found  
242 when comparing with Fig. 2c.



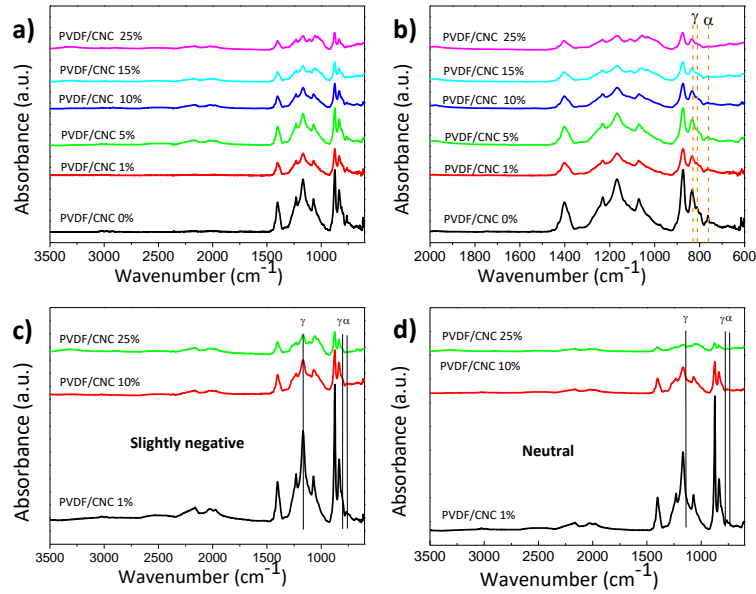
243

244 **Fig. 2.** FE-SEM micrographs of cryogenically fractured PVDF/CNC films with negatively charged CNCs  
245 at a concentration of: (a) 0%; (b) 5 % and (c) 25 %. (d) PVDF/CNC with neutral CNCs at 25 %.

246

247 To study the influence of the CNC charge on the resulting PVDF crystalline form a  
248 Fourier transform infrared spectroscopy (FTIR) analysis was performed. The infrared  
249 spectra of the PVDF/CNC nanocomposites are shown in Fig. 3. The CNC absorption  
250 bands at 3650-3200  $\text{cm}^{-1}$  are assigned to the O-H stretching vibration of CNC,  
251 indicating the presence of the CNC into the matrix [39]. As expected, an increase in the  
252 CNC characteristic absorption bands occurs when the CNC amount increases.

253 Independently of the CNC charge, the main characteristic PVDF absorption bands are  
254 observed for the different PVDF/CNC nanocomposites with different CNC charges. The  
255 absorption band at  $\sim 1403 \text{ cm}^{-1}$  is attributed to the wagging vibration of the  $\text{CH}_2$  group.  
256 The absorption bands at 796 and 760  $\text{cm}^{-1}$  are ascribed to the PVDF  $\alpha$  phase. The  
257 absorption bands at 1245, 833 and 811  $\text{cm}^{-1}$  are assigned to the  $\gamma$  phase characterized by  
258 a  $\text{T}_3\text{GT}_3\text{G}$  conformation, being an indicative that neat and PVDF/CNC nanocomposites  
259 crystallize into the  $\gamma$  phase, independently of the CNC charge [40] (observed in detail  
260 latter in the Fig. 3b). From all the FTIR spectra it is also observed the absence of an  
261 absorption band at 1275  $\text{cm}^{-1}$  [40], characteristic of the  $\beta$  phase (for PVDF having low  
262 molecular weight  $\beta$ -phase fraction decreases with increasing evaporation temperature  
263 due to different evaporation rates [41, 42]). For evaporation temperatures above 90  $^\circ\text{C}$ ,  
264 the evaporation rate is high and there is no enough time for nucleation of the more  
265 stable  $\alpha$ -phase phase, and the polymers growths into a metastable phase [42]. These  
266 results indicate that the solvent evaporation at 90  $^\circ\text{C}$  favors PVDF crystallization  
267 process into the  $\gamma$  phase crystalline structure due to significant polymer chain  
268 entanglements. It is also to notice, that independently of the CNC charge (Fig. 3c and  
269 3d), a decrease on the  $\alpha$  phase absorption bands intensity is observed, indicating that the  
270  $\gamma$  phase becomes the predominantly phase in the PVDF/CNC blends with increasing  
271 CNC content.



272

273 **Fig. 3.** FTIR spectra of PVDF/CNC nanocomposites for different CNC surface charges: a) PVDF/CNC  
 274 having negatively charged CNCs; b) enlarged FTIR spectra of PVDF/CNC with negatively charged  
 275 CNCs; c) PVDF/CNC comprising slightly negative CNCs and d) PVDF/CNC comprising neutral CNCs.  
 276

277 The influence of CNC addition on the amount of  $\gamma$  phase was quantified from FTIR  
 278 results according the following Equation:

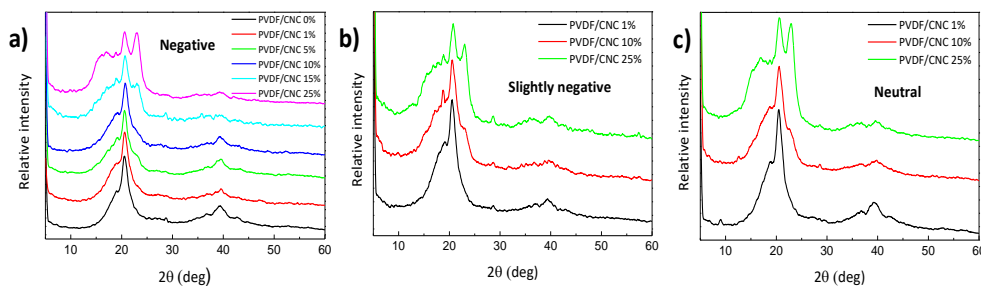
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$$F(\gamma) = \frac{A_{\gamma}}{\left(\frac{K_{\gamma}}{K_{\alpha}}\right)A_{\alpha} + A_{\gamma}} \quad (4)$$

280 where  $A_{\alpha}$  and  $A_{\gamma}$  represent the absorbencies at  $766$  and  $833$   $\text{cm}^{-1}$  corresponding to  $\alpha$ -  
 281 and  $\gamma$ -phases and  $K_{\gamma}$  and  $K_{\alpha}$  are the absorption coefficients being  $0.365$  and  $0.150$   $\mu\text{m}^{-1}$ ,  
 282 respectively [1]. As expected, neat PVDF crystallizes mainly in the  $\gamma$  phase, reaching a  
 283  $\gamma$  phase content of 86%. Similar results are observed for the PVDF/CNC blends with  
 284 different CNC charges, being observed a PVDF crystallization into the  $\gamma$  phase. For the  
 285 nanocomposite bearing negatively charged CNCs, the  $\gamma$  phase content increases up to  
 286 90% with the CNC amount increase until 5%. For CNC concentrations larger than 5%,  
 287 the PVDF tends to crystallize only in the  $\gamma$  phase as shown Table 1. Similarly, the  
 288 slightly negative ( $-26.1 \pm 3.7$  mV) and neutral ( $-4.4 \pm 0.3$  mV) CNCs induce a PVDF

289 crystallization in the  $\gamma$  phase. These results suggest that the negative charge of the CNC  
290 interacts with the PVDF  $\text{CH}_2$  groups and the positively CNC charges with the negative  
291  $\text{CF}_2$  groups. However, these interactions are weak as similar results are observed for the  
292 samples containing the neutral CNC.

293 The effect of CNC charge and concentration on the resulting PVDF crystallization  
294 has been evaluated through X-ray diffraction (XRD). Fig. 4 shows the obtained XRD  
295 patterns for the PVDF and PVDF/CNC nanocomposites comprising different charges.  
296 From Fig. 4a it is observed that PVDF displays two diffraction peaks at  $2\theta = 18.9^\circ$  and  
297  $39.4^\circ$  and a stronger peak at  $2\theta = 20.5^\circ$ . These diffraction peaks are ascribed to the  
298 PVDF  $(020)$ ,  $(211)$  and  $(110/101)$ , respectively, and are associated with the monoclinic  
299  $\gamma$  phase respectively. These results are in agreement with the FTIR results where it was  
300 observed that PVDF mainly crystallizes in this phase. Similar results are observed for  
301 the PVDF/CNC negatively charged containing 5% of CNC. For higher CNC ratios (10-  
302 25%) the diffraction peaks at  $14.9^\circ$ ,  $16.5^\circ$  and  $22.7^\circ$  are attributed to the  $(1-10)$ ,  $(101)$   
303 and  $(200)$  crystallographic planes of CNC respectively (cellulose I form), increasing the  
304 peaks intensity with the CNC amount increase [28]. Similar results are observed for the  
305 PVDF/neutral (Fig. 4b) and positive (Fig. 4c) CNC nanocomposites, where the intensity  
306 of the diffraction peaks arising from CNC increase with CNC fraction.

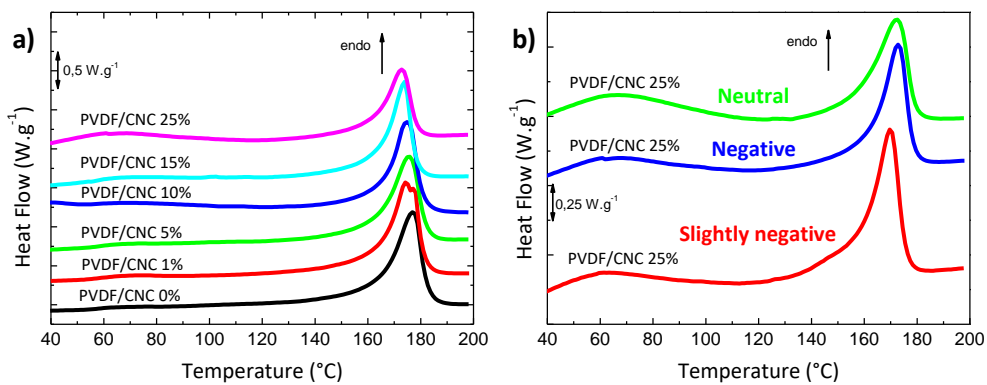


307  
308 **Fig. 4.** XRD patterns of PVDF/CNC nanocomposites for different CNC surface charges: a) negatively  
309 charged CNCs; b) slightly negative CNCs and c) neutral CNCs.

310

311 3.3. Thermal properties

312 The effect of CNC surface charge on the degree of crystallinity and melting  
313 temperature of the PVDF/CNC nanocomposites was determined by differential  
314 scanning calorimetry (DSC). Fig. 5a shows the DSC heating thermograms of  
315 PVDF/CNC nanocomposites where the endothermic curves represent the melting  
316 process of PVDF phase achieved at 170-180°C. A single peak is observed for all  
317 PVDF/CNC nanocomposites except for the nanocomposite with 1% where the existence  
318 of the double peak in the PVDF melting behavior can be attributed to the increase of  
319 lamellae thickness, i.e. the interlamella diffusion of the polymer chains [43, 44].



320  
321 **Fig. 5.** DSC thermograms for PVDF/CNC nanocomposites for different compositions and CNC surface  
322 charges: a) negatively charged CNCs and b) a comparison between PVDF/CNC 25% nanocomposites  
323 containing strongly negative, slightly negative and neutral CNCs.

324  
325 It is observed that the melting temperature of the PVDF polymer is not affected by  
326 the addition of CNC filler and its value remains between 173-177 °C within the  
327 experimental error. This behaviour is also observed for other all the nanocomposites  
328 bearing CNCs with different surface charges as shown in Fig. 5b for 25 wt% of CNC.  
329 Indeed, no changes on the thermal transitions are observed upon CNC surface  
330 modification. To get further insights on the effect of CNC surface charge on the

331 structure of PVDF, the degree of crystallinity for all PVDF/CNC nanocomposites was  
 332 determined through the following equation:

$$333 \quad X_c(\%) = \frac{\Delta H_f}{\Delta H_f^0 \cdot W_m} \quad (5)$$

334 where  $\Delta H_f$  is the fusion enthalpy measured during the heating scan,  $W_m$  is the PVDF  
 335 matrix weight fraction and  $\Delta H_f^0$  is the heat of fusion of an infinitely thick PVDF crystal  
 336 (set at  $104.6 \text{ J}\cdot\text{g}^{-1}$ ) [1]. Accordingly, Table 1 shows the degree of crystallinity for all  
 337 PVDF/CNC nanocomposites. It is observed that the degree of crystallinity remains  
 338 independent of the CNC amount and surface charge, which can be explained by the fact  
 339 that CNC filler does not act as nucleating agent and does not affect the melting  
 340 behaviour of PVDF matrix.

341

342 **Table 1.** Degree of crystallinity ( $X_c$ ) and  $\gamma$ -phase content for all PVDF/CNC nanocomposites.

Sample	$X_c \pm 3$ (%)	$\gamma$ -phase $\pm 2$ (%)
PVDF	48	86
PVDF/CNC (negative) 1%	44	90
PVDF/CNC (negative) 5%	43	100
PVDF/CNC (negative) 10%	40	100
PVDF/CNC (negative) 15%	41	100
PVDF/CNC (negative) 25%	44	100
PVDF/CNC (slightly negative) 25%	46	100
PVDF/CNC (neutral) 25%	44	100

343

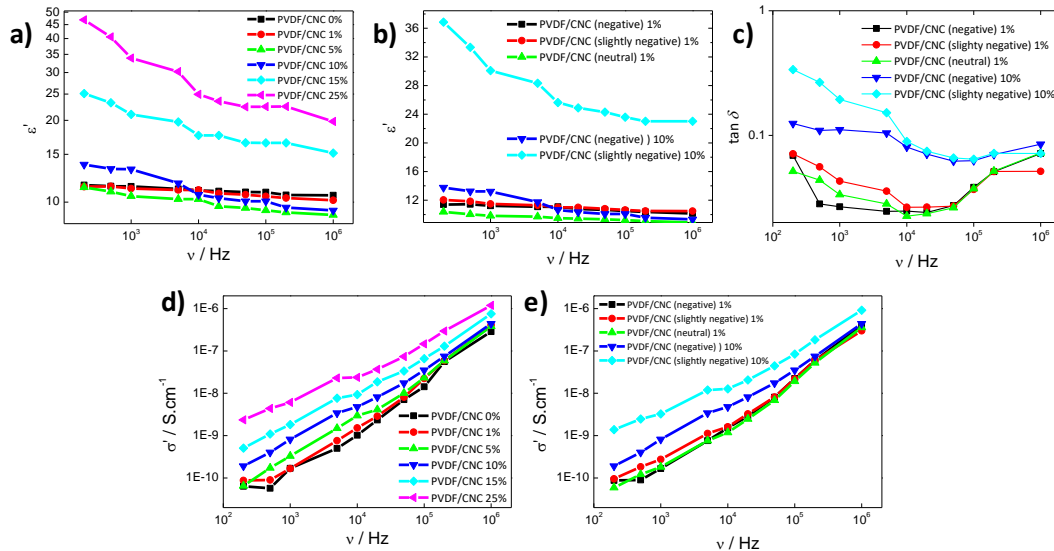
### 344 3.4. Dielectric properties

345 The dielectric behaviour of PVDF/CNC nanocomposites in the frequency range of 20  
 346 Hz to 1 MHz at 25°C was evaluated to study the effect of CNCs on the electrical  
 347 properties of the films. Fig. 6a shows the variation of the  $\epsilon'$  for all PVDF/CNC  
 348 nanocomposites with negative charge as a function of frequency. Independently of the



349 CNC amount, the dielectric constant decreases with increasing frequency as a result of  
 350 the electrical relaxation of the dipoles as frequency increases. It is verified that the  
 351 dielectric constant depends of the CNC amount as it increases with increasing CNC  
 352 content due to the increased space charge (Maxwell-Wagner-Sillier (MWS) polarization)  
 353 and polarization contributions by the hydroxyl groups (-OH) present in the cellulose  
 354 [45]. In addition, at low frequency, the high dielectric constant value for 25% CNC  
 355 content is ascribed to the large interfacial charge polarization between the PVDF matrix  
 356 and the CNC fillers.

357 For 1% of CNC, Fig. 6b shows that CNC surface treatment barely affects the  
 358 dielectric behavior of PVDF/CNC nanocomposites. For 10% of CNC, on the contrary, it  
 359 is observed that surface treatment affects the dielectric behavior as the removal of ester  
 360 groups increases the dielectric constant as a result of the presence of more polar -OH  
 361 groups that increase dipole-dipole interactions and interfacial polarization between  
 362 PVDF polymer and CNCs [46].



363  
 364 **Fig. 6.** (a) Real dielectric constant, (c) dielectric loss and (d) conductivity values as a function of  
 365 frequency for PVDF/CNC nanocomposites having negatively charged CNCs. (b) Real dielectric constant,  
 366 (c) dielectric loss and (e) conductivity values as a function of frequency for PVDF/CNC nanocomposites  
 367 having surface modified CNCs.

368

369 The dielectric loss ( $\tan \delta$ ) as a function of frequency for PVDF/CNC nanocomposites  
370 is shown in Fig. 6c. It is noticed that the dielectric tangent loss increases with increasing  
371 CNC amount due to the increased the space charge polarization associated with  
372 interfacial polarization between filler particles and PVDF polymer. For modified CNCs,  
373 the dielectric tangent loss also increases with CNC amount. It is worthy to note that for  
374 the 10% nanocomposite  $\tan \delta$  results much larger (up to an order of magnitude larger)  
375 upon CNC surface modification. This can be explained by the fact that surface treatment  
376 increases the amount of accumulated charges at the PVDF-CNC interface thanks to  
377 higher amount of the polar groups originated by treatment (sulfate half-ester removal to  
378 yield -OH groups) [47].

379 Regarding the electrical AC conductivity values represented in Fig. 6d and 6e,  
380 increased electrical AC conductivity is observed with increasing the CNC concentration  
381 and CNC surface treatment. The AC electrical conductivity increases with frequency in  
382 nearly four orders of magnitude in the measured frequency range, showing a strong  
383 contribution of confined dynamics to the electrical conductivity, compatible with  
384 Maxwell-Wagner-Sillier (MWS) polarization contributions [48-50]. For PVDF/CNC  
385 nanocomposites, the conduction mechanism occurs through the hopping of the charge  
386 carrier in localized states that increase for higher CNC concentration (Fig. 6d) and for  
387 surface treatment that increases the polar -OH groups (Fig. 6e).

388 The AC conductivity behaviour can be described by Jonscher power-law [51]:

389 
$$\sigma'(\omega) \propto \omega^n, n \leq 1 \quad (6)$$

390 where  $\omega$  is the angular frequency and  $n$  ranges between  $0 < n < 1$ , characterizing the  
391 hopping conduction mechanism [52]. For PVDF/CNC nanocomposites with negatively  
392 charged CNCs, the  $n$  value increases with CNC concentration and ranges from 0.5 to  
393 0.9 due to the increase of charge carriers in localized states. For 10 wt% of CNC with

394 different surface treatment, the  $n$  value is 0.74 to 0.80, the addition of polar groups  
395 affecting the mobility of the charge carriers.

396

### 397 **Conclusions**

398 The development of PVDF-based nanocomposites comprising surface-modified  
399 CNCs is here presented. Based on NaOH and cationization treatments, the initial highly  
400 negative CNCs arising from the sulfuric acid-induced hydrolysis leads to slightly  
401 negative and nearly neutral (zeta potential values of  $-45.2 \pm 1.1$  mV,  $-26.1 \pm 3.7$  mV and  
402  $-4.4 \pm 0.3$  mV) CNCs. Based on FTIR, XRD and DSC results, no structural changes are  
403 achieved upon the incorporation of CNCs into PVDF through doctor blade casting  
404 approach. All samples showed the presence of the electroactive  $\gamma$  phase with a  $X_c$   
405 crystalline fraction in PVDF ranging from 40 to 48 %. Dielectric spectroscopy analyses  
406 show a continuous increase on the real dielectric constant, dielectric loss and ac  
407 conductivity values after CNC incorporation due to the increase of the charge carrier  
408 concentration and ionic conductivity arising from CNCs. Interestingly, the real  
409 dielectric constant, dielectric loss and ac conductivity values can be further increased  
410 upon CNC surface modification. Such results are explained in terms of  $-\text{OSO}_3\text{H}$  group  
411 removal from CNCs, which enable the presence of additional polar  $-\text{OH}$  groups which  
412 can interact with PVDF matrix. This work provides novel cues for the development of  
413 cellulose-based multifunctional materials with enhanced electroactive response.

414

### 415 **Data availability**

416 All the data used to support the findings of this study are included within the article.

417

### 418 **Acknowledgements**

419 The authors thank the FCT (Fundação para a Ciência e Tecnologia) for financial support  
420 under the framework of Strategic Funding grants UID/FIS/04650/2019,  
421 UID/EEA/04436/2013 and UID/QUI/0686/ 2016; and projects no.  
422 PTDC/BTM-MAT/28237/2017; PTDC/EMD-EMD/28159/2017 and PTDC/FIS-  
423 MAC/28157/2017. The authors also thank the FCT for financial Support under grants  
424 SFRH/BPD/121526/2016 (D.M.C.) and SFRH/BPD/112547/2015 (C.M.C.) as well  
425 POCH and European Union. Financial support from the Spanish Ministry of Economy  
426 and Competitiveness (MINECO) through project MAT2016- 76039-C4-3-R  
427 (AEI/FEDER, UE) (including FEDER financial support) and from the Basque  
428 Government Industry and Education Departments under the ELKARTEK, HAZITEK  
429 and PIBA (PIBA-2018-06) programs, respectively, is also acknowledged

430

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