

See discussions, stats, and author profiles for this publication at: <https://www.researchgate.net/publication/351625499>

Human Error–Induced Risk in Reinforced Concrete Bridge Engineering

Article in *Journal of Performance of Constructed Facilities* · August 2021

DOI: 10.1061/(ASCE)CF.1943-5509.0001595

CITATIONS

5

READS

397

3 authors:



Neryvaldo Galvão

Infrastructure Management Consultants

20 PUBLICATIONS 89 CITATIONS

[SEE PROFILE](#)



Jose Campos Matos

University of Minho

267 PUBLICATIONS 1,178 CITATIONS

[SEE PROFILE](#)



Daniel V. Oliveira

University of Minho

370 PUBLICATIONS 6,494 CITATIONS

[SEE PROFILE](#)

Some of the authors of this publication are also working on these related projects:



HeritageCARE - Monitoring and preventive conservation of the historic and cultural heritage [View project](#)



Vernacular buildings from the Entre-Douro-e-Minho. [View project](#)

Human Errors induced risk in reinforced concrete bridge engineering

Authors:

Neryvaldo Galvão^{1*}

José C. Matos²

Daniel V. Oliveira³

Abstract:

Throughout the last century and in recent years, several bridge failures have taken place worldwide. Recent studies uncovered that the primary cause of these collapses were human errors in design, construction and operation phases. Regardless of this finding, there is still a considerable gap between this information and the known errors and the risk they represent for structural safety. Aiming for a better understanding of human errors, an identification procedure and a qualitative assessment of such errors considering risk-based indicators (probability of occurrence and consequence) was performed. Several brainstorming meetings with design and construction experts led to the identification of 49 relevant human errors, which were listed for further evaluation on a survey. Much more important than identifying and assessing these errors is identifying those that pose a greater threat to safety. Using a decision-making tool (Analytical Hierarchy Process) to process all the information collected in the survey, the errors were ranked according to risk indicators. Furthermore, a qualitative risk assessment is performed, allowing the identification of the errors denoting higher risk for structural safety, according to experts' opinions.

Keywords: Human error, Bridge Failure, Reinforced Concrete Bridges, Risk Analysis, Analytic Hierarchy Process (AHP)

¹ Ph. D candidate, University of Minho, Civil Engineering Department, Institute for Sustainability and Innovation in Structural Engineering, Guimarães, 4800-058, Portugal. Email: neryvado.galvao17@live.com *(corresponding author)

² Assistant Professor, University of Minho, Civil Engineering Department, Institute for Sustainability and Innovation in Structural Engineering, Guimarães, 4800-058, Portugal. Email: jmatos@civil.uminho.pt

³ Associated Professor, University of Minho, Civil Engineering Department, Institute for Sustainability and Innovation in Structural Engineering, Guimarães, 4800-058, Portugal. Email: danvco@civil.uminho.pt

32 **Introduction**

33 As one of the key elements for economic growth and citizens' well-being, the transportation sector has always
34 been a valuable asset for societies. Nevertheless, the transportation system depends very often on connections
35 provided by roadway, railway, and footway bridges. Thus, these infrastructures play a crucial role in the
36 transportation network, being responsible for tremendous consequences when wrongly managed. Several
37 examples can be found in the literature (Cavaco, 2013; Imhof, 2004; Scheer, 2010). According to design standards
38 (CEN, 2005; ISO, 2015; JCSS, 2001), a structure shall be designed and executed in such a way, with an appropriate
39 degree of reliability and robustness, that it will not be damaged to an extent disproportionate to triggering events
40 such as explosion, impact and consequence of human errors. Aiming at the reduction of occurrence rate and
41 consequence of bridge collapse, the reliability and robustness of these structures should be increased (Starossek
42 and Haberland 2010), as well as the identification of the sources of uncertainties and triggering events that may
43 lead to their failure.

44 Relying on the work developed by (Syrkov, 2017) and further developed within task group 1.5 of the
45 International Association for Bridge and Structural Engineering (IABSE), statistics in bridges failure will be
46 briefly discussed. Such a database is probably the most relevant bridge failure database available with more than
47 700 bridge failure incidents worldwide from 1966 to 2018 and covering the leading causes of failure. Examining
48 the information provided by the database, it is concluded that the main source of uncertainties triggering bridges
49 collapse is human errors (see Fig. 1). The design and construction errors are responsible for 31.8% of the collapses,
50 while the operation errors are responsible for 32.2%.

51 Several definitions have been given to human errors in the literature. Nevertheless, due to its broad scope, a
52 formal definition is required, leaning toward its boundaries definition to prevent misunderstandings with other
53 works definitions. Within the scope of this paper, human errors are any Procurement, Design, Construction and
54 Operation errors (deviations out of the acceptable margins) that do not exceed the currently available engineering
55 knowledge and have taken place due to poor work condition, lack of knowledge, negligence, miss instruction and
56 communication, greed, calculation errors, time and budget constraints, inadequate construction methods, lack of
57 surveillance, among others. Such errors or uncertainties are not covered by the partial safety factors given in
58 present-day semi-probabilistic standards. A similar understanding of what is understood by human errors is shared
59 by (Stewart & Melchers, 1988; Tylek, Kuchta, Rawska-Skotniczny, 2017, Brehm & Hertle, 2017). Also, aiming
60 the explanation of human errors boundaries, its clusters are schematically presented in Fig. 2. Human errors and

61 human-made hazards are two major components of human factors field, being the former the interaction of humans
62 with a system as a technician, and the later the interaction of humans with the system as a user.

63 By performing a more exhaustive analysis over the database, aiming at a more detailed analysis of the causes of
64 failure of reinforced concrete bridges, some relevant specific failure causes are presented in Fig. 3. Each of these
65 specific failures causes are linked to the main ones as follow: (a) Natural hazards (floods and wind effects); (b)
66 Human-made hazards (ship collision, explosion, vehicle collisions, vandalism, and overloading by live load); (c)
67 Design and construction errors (design defect, construction defect, design and construction defects and
68 construction negligence); (d) Operation errors (corrosion, deterioration of reinforced concrete, and overloading by
69 the live load (during maintenance works)). A similar classification of the causes of the collapse of bridges can be
70 found in (Deng et al. 2016; Imhof, 2004). Some specific causes of failure such as debris in the water, creep and
71 shrinkage, temperature, normal corrosion, and freeze-thaw cycles with small percentage were gathered into the
72 group named Others. One can observe from Fig. 3 that flood is responsible for a considerable number of failures,
73 and due to climate change, its influence is likely to increase due to increasing rainfall intensity (Chen 2017). More
74 detailed research on flooding effects (namely scour) uncertainties can be found in (Johnson et al. 2015; Manfreda
75 et al. 2018).

76 **Procurement errors**

77 The procurement phase is defined by the explanation of the overall idea of an undertaking, definition of execution
78 deadlines suitable for the owner, forecast of the overall cost of the project and selection of the technical team
79 (designer and contractor). The incorrect management of the procurement phase very often leads to poor decision
80 making from the owner, creating and stimulating several sources of the errors taking place in the design,
81 construction and operation phase.

82 Given the highly aggressive labour market, companies from the construction industry sometimes face decisions
83 where they are forced to assume execution time and financial costs beneath the needs for the proper fulfilment of
84 the durability, safety or serviceability requirements. Hence, the technical expertise and technology required for
85 successful design and execution are not always the key factor for the contractor or the designer eligibility. The
86 restricted execution time and limited resources usually lead to simplification of complex tasks that typically require
87 expertise and detailed approach, leading very often to assumptions that do not correspond to the reality nor reliable
88 execution strategies. Therefore, many of the errors that might occur in the later stages of a project are often the
89 consequence of the procurement phase's primary mistakes. Quality control strategies are also features of the

90 procurement phases that can greatly impact the identification and mitigation process of potential sources of errors.
91 Thus, a balance between reasonable execution time, cost, quality control strategies and the selection of a qualified
92 technical team (enough experience) should be set as a strategy for human error mitigation in the long term.

93 **Design errors**

94 **Conceptual errors**

95 The conceptual stage considers several essential aspects required for a successful design. Aspects such as the
96 contextualization of the design project in time and space, considering the available engineering technology,
97 adequate base material at disposal, maximum concrete strength manufactured with local raw materials, reachable
98 technical and non-technical support, suitable structural system and construction procedure (according to
99 geotechnical constraints) and required geotechnical characteristics. All these aspects influence the cost of the
100 project and the complexity of execution, consequently providing a greater or lesser environment for human errors
101 occurrence (Fröderberg, 2015). Hence, a well-achieved conceptual design is also a mitigation strategy of human
102 errors induced risk. Such considerations should demand an even greater consideration when the project is of non-
103 local or international nature since the designer and the contractor must get familiar with local needs and safety
104 requirements.

105 A well achieved conceptual design pays off in the long run, by a good structural performance during its
106 operation, minimization of the structure life cycle costs and robust performance under expected or even unexpected
107 single or multiple hazards. Projects with a daring conceptual design with large spans, uncommon column and deck
108 shapes, and other unique characteristics are more vulnerable to human errors, requiring utmost attention and
109 mitigation measures. For conventional bridges though, the conceptual design is a more standardized procedure
110 since agencies already established internal specifications dictate the material, span, structural systems, among other
111 features of the structure. Thus, a less error-prone design is to be expected. A good example of a well-achieved
112 conceptual design, leading to the reduction of a human-made hazard probability of occurrence, is the consideration
113 of an arch bridge instead of a common girder bridge with several piers to avoid vessels collisions on the piers. This
114 example is given in a context where the bridge would span over a river/narrow sea with high traffic. The definition
115 of a structural system compatible with construction procedure or technique usually employed by contractors is
116 also a good conceptual strategy aiming to reduce execution difficulties.

117 **Structural analysis and design errors**

118 Nowadays, international demand over the construction industry requires design corporations to be involved in
119 numerous projects worldwide. Under this scenario, local standards must be used during the design very often, and
120 the philosophy behind them may be varying from one to another. The same standards can be occasionally
121 incomplete, leading to the need for the combination of different standards. Errors scenarios are drawn, mostly
122 when the quantification of design loads is completed using a given standard where safety factors are less strict in
123 the quantification of the design loads than in the resistance computation. Simultaneously, the resistance
124 computation is performed according to a different standard where the philosophy behind it is the opposite.
125 Consequently, the structural reliability due to these standards' combination will be below the target values
126 established initially by both standards. Non-coherence between several international design codes was reported by
127 (Sykora et al. 2017), where different target reliability values are recommended for the same case study.

128 Another common source of error is in the definition of the structure boundary conditions or the soil-structure
129 interaction due to high uncertainties linked to soil behaviour when wrongly addressed. Foundation rotations,
130 differential settlements, support condition stiffness and geotechnical failure, are issues that require careful
131 evaluation from experts, but sometimes neglected, even though they are responsible for tremendous consequences.
132 Other issues, such as mistaken allocation of the bearing devices and lack of maintenance leading to support
133 condition different from the initially designed, can lead to a severe structural system malfunctioning. A common
134 example used to demonstrate the importance of the previously mentioned matter is the development of second-
135 order effects in bridges with long piers due to the development of friction forces between the deck and the
136 malfunctioning bearing devices, caused by the deck thermal expansion or shrinkage. As the bearing device allows
137 the deck to deform freely at the design stage, the second-order effects are typically not considered for strength
138 computation.

139 During the construction and transportation of structural components, a structural element or the structural
140 system itself goes through different static conditions that are often different from the final ones considered in the
141 design. Therefore, the structural system or the element resistance might be tested in certain cross-sections not
142 designed to support unexpected stresses. Precast and prestressed elements are often damaged by the failure of
143 decompression limit state caused by this error, leading to premature cracks. Nevertheless, more severe
144 consequences such as element yielding or system collapse may also occur, especially when the construction
145 technique demands static conditions changings during different assemble steps.

146 **Detailing errors**

147 All the information gathered and created by the designer is transferred to the main contractor through detailed
148 drawings. Through the detailing phase, two stakeholders with different mindset are deeply connected; hence, the
149 information conveyance must be clear to avoid any misinterpretation of the high volume of information being
150 transferred. These are common characteristics of all linking and interface activities. As an interface or linking
151 activity, detailing is considered a potential source of errors since it is susceptible to a mistaken interpretation of
152 the given information, absence of specific information, drawings mistakes, among other errors. As such, the
153 detailing phase should be carefully managed, especially when the information being transferred is of great
154 importance for structural safety.

155 During the structural analysis and design, several assumptions are made, and very often, these assumptions
156 play a crucial role in the successful performance of a system. It is not uncommon to find detailing drawings where
157 the detailing strategy does not agree with the standard recommendations for the previously considered design
158 assumptions, leading to unpredicted behaviours. For instance, systems with some redistribution capabilities are
159 usually proposed in seismic design. Thus, the connection between different structural elements is expected to have
160 improved ductile behaviour; hence, specific detailing strategies should be used, so the structural analysis
161 correspond to the structure performance as built.

162 **Construction errors**

163 **Falsework execution errors**

164 Falsework or scaffold execution errors are referred to as being the most commons errors and responsible for the
165 worst consequences in the execution phase. They often lead to complete demolition of concrete elements and a
166 high number of fatalities and injuries. A flawed assessment of the falsework foundation, or no assessment at all
167 going beyond the visual inspection, is a common problem. It is not unusual to find an execution plan where the
168 collected data from piers or abutments foundation location are used to check the falsework foundation resistance.
169 This procedure may fail when the falseworks are needed in extended lengths, because the foundation's geotechnical
170 properties may vary along its length, especially if the given soil is heterogeneous, leading to soil properties
171 assumptions entirely dissimilar to the real one. This mistaken assumption may well end up in substantial
172 settlements, converted into large deflections, or even structural collapse. Another likely scenario of failure is the
173 non-consideration of the reduction of soil resistance due to rainfall conditions. For this auxiliary structure, the area

174 through which the load is transferred to the ground is usually small; thus, the soil stress limits should be carefully
175 controlled. A common mistake here is the use of soil maximum load capacity as its resistance performance
176 indicator, neglecting the importance of the area through which the load is transferred.

177 Movable falseworks require utmost attention when changing them from their current position to a new one
178 since a constant change in its support condition is necessary. As such, no room for mistakes is allowed given severe
179 consequences that might take place. Collapses have taken place in several constructions using this technic due to
180 miss coordination between the different involved parts and lack of proper surveillance and effective
181 communication.

182 **Material quality control errors**

183 Nowadays, material quality control errors are becoming a less concerning issue due to the industry's rigorous
184 standards adopted to avoid former misfortunes and for quality assurance purposes. Nevertheless, this was not a
185 certainty during the last century. The exceptional registered occurrences are related to concrete quality
186 specifications due to a mistaken evaluation of aggregates water content, alkali-aggregate reaction, wrongful
187 quantification of the required admixtures, and miscalculations to fulfil specific concrete requirements (e.g.
188 concrete strength, elasticity modulus, among others). It is also worth mentioning the deficient vibration of concrete
189 in areas of difficult access, due to high density of passive and active reinforcement allowing the formation of voids,
190 or excessive vibration leading to segregation of concrete constituents. Additional deformation of concrete due to
191 non-agreement between creep properties of employed concrete with those assumed in the design, is an error to
192 bear in mind. Concerning the durability, it has been reported that the usage of the right or favourable use of the
193 cement type can double the service life of the structure (Zambon et al., 2019). In construction sites where more
194 than one reinforcement class is available, it is vital to take these classes' incorrect usage as a potential risk.
195 Additionally, proper storage condition of reinforcement to avoid early corrosion and ductility reduction is an
196 important consideration to keep in mind, especially when a long-stored period is concerned. Also, a non-controlled
197 concreting of mass concrete components leading to high temperature is an error that leads to deficient concrete
198 with severe strength reduction.

199 **Logistics errors**

200 The construction phase requires massive management of human, equipment, and material resources. Thus, logistic
201 errors are part of companies' daily work, and they must not be neglected. Some examples are here presented:

- 202 - Adoption of a concrete resistance class or other specification that is not available at an affordable distance
- 203 from the construction site;
- 204 - Air pollution, underground water or soil contamination, due to inadequate eco-friendly safety measures;
- 205 - Functional capabilities limitations of movable and fixed cranes in the construction site due to errors
- 206 related to insufficient foundation preparation, limited action radius, allowed movable distance, maximum
- 207 transportation weight, among others;
- 208 - Absence of special licences for transportation of big precast elements through public roads or physical
- 209 restrictions to transportation can be a drawback that usually turns into large delays;
- 210 - Inadequacy of the launching girders to the pier's geometry is a logistic error to keep in mind;

211 **Bridges collapse**

212 Particular major bridges collapse were recorded due to some of the errors highlighted in the previous section.
213 Given their technical relevance, they are shortly described and discussed.

214 In early 2018, one of the towers of a reinforced concrete cable-stayed bridge under construction in Colombia
215 (Chirajara) collapsed due to a design error. The same error also led to the demolition of the still-standing tower
216 since it was also about to collapse, making any attempt for its strengthening or rehabilitation very problematic.
217 Ten workers lost their lives during the incident, and another five injured required some medical support. An
218 investigation about the incident headed by Modjeski & Masters concluded that the bridge collapse was caused by
219 the failure of the prestressed transversal girder and the failure of the diamond tower lower diaphragm. The
220 influence of the tower diaphragm, in its overall resistance, was overestimated at the design stage (Bridge Design
221 Engineering, 2018). Other sources state that the prestressed transversal girder was insufficiently prestressed and
222 that the main reinforcements of the tower diaphragm were placed in the wrong direction (Pujol et al. 2019).

223 On March 2018, a pedestrian bridge under construction in the USA (Miami) collapsed due to a design error
224 causing six deaths and eight injuries. It was reported by the Federal Highway Administration Office of Bridges
225 and Structure that a design error led to the overestimation of the stresses that could be taken by the bridge. The
226 cracks observed before the collapse were consistent with the design error. Lab tests were performed over the
227 concrete samples to check its quality, proving that the concrete met the standard's requirements (NTSB, 2018).
228 The bridge had structural design deficiencies that contributed to the collapse during one of the construction stages.
229 The consultant hired by FIGG Bridge Engineers (the engineer of record) to conduct an independent peer review
230 of its design did not check the structural integrity of the bridge for different construction stages. Consequently, the

231 review was performed only under the final design stage, where all segments of the bridge were already in place
232 and completed (Ayub, 2019).

233 On August 2018, a cable-stayed bridge from the sixties, designed by Ricardo Morandi, collapsed in Italy
234 (Genoa) during a heavy traffic day causing 43 deaths. The collapse was mainly triggered due to structural
235 deterioration caused by advanced corrosion in one of the four cables. Despite this fact, the structure had an initial
236 deficiency related to lack of structural redundancy (absence of multiple load paths) or, consequently, lack of
237 robustness because it had few crucial supports (four cables on each tower supporting the deck). The structure had
238 another initial flaw that led to the crack of the protective concrete coat surrounding the stayed steel cable that left
239 it unprotected, unchaining a premature corrosion process. An unneglectable piece of the puzzle is also the
240 consequence of political decisions regarding public infrastructures when maintenance and restrictions applied to
241 the structure are concerned. A good example of this last statement is the Morandi bridge since a political or owner
242 decision neglecting the information given by experts also contributed to the bridge collapse (The New York Times,
243 2018). The lack of structural robustness (disproportionate outcome due to any support failure) is here highlighted
244 as a conceptual structural error once a different cable-stayed structural system with multiple load paths would
245 avoid such a terrific ending. The high rate degradation of the southern cable is here seen as an error of operation
246 since no maintenance action on the structure was taken, before an obvious indication of high degradation that was
247 prompted by a design error (protective concrete coat surrounding a highly tensioned element) from the early ages
248 of the structures (Morgese et al. 2020). Three main groups of human errors led to this catastrophic ending: the
249 conceptual error, the design error and the operation error. The occurrence of multiple errors, creating a sequence
250 of events leading to bridges collapse, is the typical scenario.

251 Despite today's efforts and the new standards for quality control that implicitly deals with human errors, these
252 errors are still a major concern. It is also known that bridge quality control standards were less strict during the
253 sixties, seventies and eighties, where a high volume of bridges was built. Therefore, in the present days, it is
254 important to consider human errors in infrastructure management procedures, in particular, when the error is
255 expected to increase the deterioration rate of the structure since maintenance strategies and interventions are
256 supported by predefined degradation rates (predictive models).

257 **Design and Construction Errors Investigation**

258 The risk management process aims at the systematic use of available information, within a carefully established
259 and clearly defined context, to identify hazards and estimate the risk they pose to human beings, property, and

260 environment. Hence, three steps are initially required (i) Hazard identification, (ii) Probability of occurrence
261 analysis, and (iii) Consequence analysis. The combination of the last two provides the risk measure. Probability
262 of occurrence and consequence analysis can be performed using a qualitative or a quantitative approach, yet the
263 later is more complex and usually employed after the first one. A hazard is defined as any condition, circumstance
264 or action that can undermine the structural system resistance features and may lead to malfunctioning or failure of
265 the structure (Canisius et al. 2011; Faber, 2008; Rausand, 2011). Within the scope of this paper, human errors are
266 the leading hazard under assessment, being design and construction errors in reinforced concrete bridges the focus
267 subject. Therefore, the novelty of this research lies in the identification of design and construction errors that are
268 carefully addressed according to expert judgement.

269 **Delphi technique and survey**

270 For hazard identification purposes the Delphi technique is here employed. The Delphi technique is defined in ISO
271 31010 (ISO, 2009a) as "a procedure to obtain a reliable consensus of opinion from a group of experts through a
272 standardized procedure". Experts are expected to express their opinions independently and anonymously while
273 having access to the other expert's views as the procedure goes on. Accordingly, six experts (20 years of average
274 work experience) were selected and questioned about the most common and troubling design and construction
275 errors in reinforced concrete bridge engineering that they have faced during their professional career. The experts
276 were asked to keep in mind a standard roadway overpass with three spans of 68 m (18 m + 27.8 m + 18 m, which
277 is the most common type in the Portuguese road transportation network). This request aimed to narrow the
278 discussion around conventional bridges, avoiding particular structural types as suspension, cable-stayed and large
279 span arch bridges. Nevertheless, the content of the information provided by the experts exceeded, to a small extent,
280 such expectation. The expert views converged to a group of 20 design and 29 construction errors, see Table 1 and
281 Table 2, respectively, clustered according to Fig. 4. The concerns expressed in the preceding chapters are also a
282 summary of the expert's thoughts.

283 Following the detailed discussion around design and construction errors and listing of such errors by experts
284 (i.e. hazard Identification), the second and third steps of the risk analysis are achieved through a survey addressed
285 to experts aiming the qualitative assessment of the probability of occurrence and consequence of such errors
286 according to five categorical levels. The experts were also encouraged to suggest additional errors important to be
287 considered. The survey was carried out by e-mail through the COST Action TU 1406 network and to additional
288 Portuguese civil engineers. The answers provided by the participants were analysed using a multi-criteria decision-

289 making tool named the analytic hierarchy process (AHP) and a risk matrix. Twenty-four participants, with
290 professional experience ranging between 5 and 40 years, answered the survey call. Half were from Portugal and
291 the other half from other European countries. Half of them were design engineers, and the other half were
292 construction site engineers, but some of them had experience in both fields.

293 **Analytic hierarchy process**

294 The AHP is a multi-criteria decision-making tool (Saaty & Vargas, 2013) that considers pair-wise comparisons of
295 alternatives and criteria to prioritize such alternatives or criteria. It is supported by qualitative or quantitative inputs
296 comparing different objects/subjects. Such comparison is numerically represented by a matrix comparing the
297 alternative i with alternative j . The AHP is typically implemented in three main steps: (i) decomposition; (ii)
298 comparative judgment; (iii) synthesis of priorities (Thompson et al. 2006). The decomposition is the
299 particularization of the problem into different choices or possible solutions, which in this paper are the design and
300 construction errors listed in the survey. The comparative judgment is performed by the survey participants where
301 the probability of occurrence (PO) and consequence (CO) of each of the errors are categorized into five levels (see
302 Fig. 5 and Fig. 6). The comparative judgement is then transformed into a comparison matrix that will allow the
303 synthesis of priorities through the matrix eigenvectors, leading to the ranking of the errors according to their
304 probability of occurrence and consequence, given the survey participants inputs.

305 The AHP is implemented through a MATLAB script developed according to Goepel's methodology (Goepel,
306 2013, 2018), aiming at a more automatized procedure to analyse the information collected through the survey.
307 Such methodology is being widely used by the research community (e.g. Kifokeris et al. 2018) given its simplicity,
308 straightforward tutorials and Excel templates available in (Goepel, 2013). The methodology is summarized here
309 into the following consecutive steps:

- 310 1. The pair-wise comparison is summarized in a square comparison matrix, rating the probability of
311 occurrence and consequence of each error using a qualitative typical 5-point Likert scale ranging from
312 one to nine or from one to the inverse of 9 (i.e. 1-3-5-7-9 and 1-1/3-1/5-1/7-1/9). One is used when errors
313 are similarly likely to occur, or similar consequences are to be expected, and nine is used when an error
314 is much more likely to occur than another one, or a much greater consequence is expected from one error
315 to the other. The inverse numbers are used when the error is less likely to occur, or minor consequence
316 should be expected when compared to another error. The comparison matrices of each participant were
317 all considered consistent.

318 2. The consolidation of each expert input is achieved by an aggregated square comparison matrix,
 319 considering the weighted geometric mean method according to equation (1), where: $a_{ij(k)}$ is the
 320 comparison performed according to Likert scale comparing error i to error j by expert k ; and w_k is the
 321 expert weighting factor defined according to its years of experience as follow i) 1.0 for 5 to 10 years of
 322 experience; ii) 1.5 for 10 to 20 years; iii) 1.75 for 20 to 30 years; iv) 2.0 for 30 to 40 years.

$$C_{ij} = \exp \frac{\sum_{k=1}^K w_k \ln a_{ij(k)}}{\sum_{k=1}^K w_k} \quad (1)$$

323 3. In order to quantify the agreement or homogeneity between different experts input, a consensus index is
 324 computed, ranging the consensus between expert's opinions from 0% (no agreement) to 100% (perfect
 325 agreement). Finding a reasonable rate of this index is crucial to support the claim of a satisfactory
 326 convergence in the identification of relative priorities of the errors. The consensus or group judgement
 327 dispersion is derived from the consensus index S^* , computed according to equation (2).

$$S^* = \frac{\left[\frac{M - \exp(H_{\alpha \min})}{\exp(H_{\gamma \max})} \right]}{\left[\frac{1 - \exp(H_{\alpha \min})}{\exp(H_{\gamma \max})} \right]} \quad \text{where } M = \frac{1}{\exp(H_{\beta})} \quad (2)$$

328 Where: H_{β} Shannon entropy beta measures the variations of priorities distribution among experts, given
 329 by equation (3). Which is dependent on Shannon entropy alpha H_{α} and gamma H_{γ} . The first one measures
 330 the average individual expert priority distribution among the errors, computed for all K experts and the
 331 second one measures the group aggregated priorities. The Shannon entropy alpha and gamma are
 332 computed according to equation (4), where p_{ik} is the normalized priority value of the i th error according
 333 to the k th expert, given by equation (5). The absolute priority values r_i are computed according to the
 334 row geometric mean method, as shown in equation (6) where N is the total number of errors.

$$H_{\beta} = H_{\alpha} - H_{\gamma} \quad (3)$$

$$H_{\alpha} = \frac{1}{K} \sum_{k=1}^K \sum_{i=1}^N -p_{ik} \ln p_{ik} \quad \& \quad H_{\gamma} = \sum_{k=1}^K -\bar{p}_k \ln \bar{p}_k \quad \text{where } \bar{p}_k = \frac{1}{N} \sum_{i=1}^N p_{ik} \quad (4)$$

$$p_i = \frac{r_i}{\sum_{i=1}^N r_i} \quad (5)$$

$$r_i = \exp \left[\frac{1}{N} \sum_{j=1}^N \ln(a_{ij}) \right] \quad (6)$$

335 Subsequently, the minimum Shannon alpha entropy H_{amin} and the maximum Shannon gamma entropy
336 H_{gamma} must be computed applying the equation (7) and equation (8), respectively. Where $c_{max} = 9$ is
337 the maximum value of importance rating used according to 5-point Likert scale to build the pair-wise
338 comparison matrix in step 1.

$$H_{amin} = -\frac{c_{max}}{z} \ln\left(\frac{c_{max}}{z}\right) - (N-1) \frac{1}{z} \ln\left(\frac{1}{z}\right) \quad \text{with } z = N + c_{max} - 1 \quad (7)$$

$$H_{gamma} = (N-K) \left(-\frac{1}{z}\right) \ln\left(\frac{1}{z}\right) - \frac{u}{z} \ln\left(\frac{1}{Kz}\right) \quad \text{with } u = K + c_{max} - 1 \quad (8)$$

339 4. Priority values are obtained by computing the eigenvector of the pair-wise comparison square matrix.
340 The prioritization or ranking of the errors is displayed in Table 1 and Table 2, last two columns, for each
341 risk indicator, that is, the probability of occurrence (PO) and consequence (CO). Relative ranking position
342 numbers are used, where the number one is attributed to the error that is more likely to occur or the error
343 expected to have the highest consequences, while the maximum number is assigned to the error that
344 represents the lowest probability of occurrence or the lowest consequence.

345 The consensus index obtained according to the AHP was 87% among the design engineers, and 73% among the
346 construction site engineers. Thus, expert opinions did not disperse too much. The awareness and resemblance of
347 the design engineer's assessment, of the design errors, are higher than those provided for the construction site
348 engineers for the construction errors. Given that the designer's daily activities go through a more standardized
349 procedure, a higher consensus index for the design engineers is a reasonable observation.

350 The input of each expert was weighted according to their years of experience. For instance, the input of a
351 structural engineer with additional professional experience should have more influence on the outcome than the
352 contribution of a junior engineer. As it is very difficult to quantify the influence of professional experience in this
353 matter, there is no way to validate the weighting factors adopted in equation (1) without performing a major study
354 of the topic. However, it is known that a senior engineer is more likely to make a better decision than a junior
355 engineer due to the accumulated expertise; therefore, the weighting factor was increased with the years of
356 experience.

357 **Qualitative risk analysis**

358 Once the design and construction errors rankings are established according to the probability of occurrence and
359 consequence, it is of paramount importance the characterization of the relationship between these two for
360 qualitative estimation of the risk. Hence, the risk matrix approach is employed (Rausand, 2011). It is commonly

361 used to rank hazardous events according to their significance, to screen out insignificant events, or to evaluate the
362 need for risk reduction of some events".

363 The loss of the information, concerning the qualitative levels assigned to the errors by the experts, is one the
364 AHP handicap. In other words, the priority list or ranking is set with a great cost since the qualitative level of each
365 one of the errors becomes unknown during the AHP procedure. The loss of such information renders difficult the
366 qualitative assessment of the error with a risk matrix. To overcome this drawback, and accomplish a broader
367 analysis of the information provided by the survey participants, the qualitative levels assigned to each risk indicator
368 are obtained for each error using a weighted geometric mean method to aggregate the participant's inputs. Fig. 5
369 and Fig. 6 show the qualitative risk matrices of the design and construction errors, respectively, and their
370 distribution according to their likelihood and expected consequences, using their identification number (ID)
371 provided in Table 1 and Table 2. The prioritization information obtained by the AHP is also considered inside each
372 matrix cell.

373 Making use of the information provided by the AHP and risk matrix, comprehensive risk classification of the
374 errors was achieved. For exemplification purposes, let one take the errors with ID7 ($PO_{\text{Ranking}} \rightarrow 7$ and
375 $CO_{\text{Ranking}} \rightarrow 18$) and ID8 ($PO_{\text{Ranking}} \rightarrow 1$ and $CO_{\text{Ranking}} \rightarrow 16$) from the design risk matrix. They are both within the
376 high-risk group ($40 \geq Risk \geq 25$), but if the AHP ranking information is taken into account, the error with ID8
377 can be highlighted as the one representing greater risk, since it has a higher ranking position than the error with
378 ID7. Therefore, the wrong definition of a cross-section shear centre (design error ID7) represents a lower risk than
379 a wrong quantification of the effects of deck deformation due to creep, shrinkage and temperature variation, in
380 columns leading to unexpected second-order effects (design error ID8). Using this same procedure, a further
381 distinction between the risk of the different errors within the same cell is possible. Nonetheless, the risk of errors
382 can be easily categorised into five different risk levels.

383 Based on Epaarachchi (Epaarachchi & Stewart, 2004), the error magnitude is the size of the error as a
384 percentage of the correct outcome or in other words; it is the parameter that describes the severity of the error. It
385 is a vital characteristic of an error, here neglected. The severity of an error is always associated with its
386 consequence but is not the ultimate factor. For instance, the consequence of error with ID8 increases with the
387 slenderness of the column, thereby, the same error with the same magnitude (equal relative deviation from its
388 correct value) might have entirely different consequences for different structural systems or components.
389 Subsequently, it is important to consider the magnitude of the error in a detailed structural analysis, mainly if the

390 error is understood as being of paramount importance for risk management. Some research work addressing error
391 magnitude can be found in the literature (Epaarachchi & Stewart, 2004; Fröderberg, 2014; Galvão et al. 2019;
392 Nowak & Collins, 2000). Nevertheless, such analysis is beyond the scope of this paper, which addresses a general
393 approach for categorization of errors according to five risk levels considering their probability of occurrence and
394 expected consequences.

395 An essential characteristic of the risk matrix here used is that it enhances the influence of the consequence over
396 the probability of occurrence, in terms of risk rating. Such a risk matrix was chosen for this research because it is
397 directly connected with risk management of civil engineering activities. Dissimilar risk matrices can be found in
398 the literature (Rausand, 2011). However, in civil engineering, the consequence should be enhanced over the
399 probability of occurrence an event in risk quantification.

400 **Additional errors collected within the survey**

401 Besides the errors listed above, the inquired experts reported a series of other errors (see Table 3 and Table 4).
402 They were not considered in the risk analysis since different experts independently reported them; thus, insufficient
403 information for the analysis was available. Nevertheless, it is important to make them available in the literature
404 for further research.

405 **Investigation remarks**

406 Looking at the risk matrices (see Fig. 5 and Fig. 6), three errors stand out in the critical zone ($Risk \geq 50$), one in
407 design errors risk matrix (ID 14) and two in the construction errors risk matrix (ID 19 & 21). The error with ID
408 14, described as the lack of consideration of different support conditions through which the element or the
409 structural system will be subjected during the construction procedure for validation of the design calculation, is
410 identified as the error that might represent the highest risk in the design phase, within the context described in this
411 paper. Coincidentally, it is the main cause of the Miami bridge collapse described in “Bridges collapse” section that
412 took place in March 2018. The construction errors found in the critical zone are both concerning the falseworks.
413 One is related to continuous bracing required for the global stability of the falsework. The other is associated with
414 the poor assessment of the foundation soil properties supporting the falsework, neglecting water influence in such
415 properties. Such negligence is common since the falsework is just a temporary structure and further investigation
416 addressing such an issue is usually not performed.

417 For summary purposes, the top five design and construction errors are listed in Table 5, according to the
418 investigation described in this paper (AHP and Qualitative risk analysis). Many errors related to
419 falsework/scaffolding take the lead in the risk analysis, along with the soil properties and support conditions.
420 During the brainstorming meetings, the malfunctioning of structures was primarily linked to these errors, since
421 they bear support to whatever is going to be built up, hence of remarkable consequences. Detailing of
422 reinforcement and lack of consistency between the design assumptions and detailing rules are two detailing errors
423 that are among the ones representing the highest risk.

424 The design error identified as the most frequent error is the incorrect quantification of the effects of deck
425 deformation due to creep, shrinkage and temperature variation in columns, causing and amplifying second-order
426 effects (ID 8). On the other hand, the least frequent error is the mistaken dead load quantification (ID 4). Within
427 the construction phase, reinforcement covering errors (ID 13) are the second most frequent errors followed by
428 expansion joints deficiency (ID 9).

429 **Human error mitigation**

430 Mitigation measures against human errors control exhibit a vast scope due to the multidisciplinary partners playing
431 different roles in this matter. From the political decision, economic constraints, cultural and environmental
432 influences, missing technological advancements of the sector, the engineers' qualification, the type of structural
433 systems and geometric shapes used, makes very difficult any attempt to provide specific mitigation measures
434 without bringing forth a long discussion that goes beyond the scope of this work.

435 The increase of the awareness of design and construction errors and the discussion around the subject and their
436 risks is a mitigation strategy itself since the mitigation of known potential hazards, and their risks are part of
437 engineers' daily challenges.

438 A few common mitigation measures were pointed out by the experts consulted within the scope of this research,
439 namely the use of different design software for outputs validation, critical interpretation of the outputs by expert
440 engineers, self-made computation sheets for validation of the software outputs, the careful appointment of the
441 project surveillance team and serious investigation of the geological and geotechnical properties of the foundation
442 soil.

443 In civil engineering, the uniqueness of each construction and its details render challenging to approach the
444 problem in terms of production automation. However, with artificial intelligence, there might be a greater influence

445 of technology in the construction sector for human errors mitigation. Nowadays, contractors are continuously
446 gathering data on accidents taking place in the construction site, so machine learning can be used to find underlying
447 patterns in the collected data and prevent accidents (engineering .com, 2019; Kifokeris & Xenidis, 2019; Maskin
448 entreprenoren, 2020). Nevertheless, other technological advancements are already playing an important role in this
449 matter these days, through technologies such as Building Information Modelling Technology, 3D printing, Virtual
450 Reality and Augmented reality (Qeshmy, Makdisi, Ribeiro da Silva, & Angelis, 2019). From the economic point
451 of view, investments in such innovative technologies are compensated because a problem found during the design
452 phase that cost 1\$ to fix, will cost 20\$ to fix during the construction phase and 60\$ to fix during the operation
453 phase (engineering .com, 2019).

454 **Quality management measures**

455 Basic design, execution and maintainability requirements are the foundation of design codes such as the
456 Eurocodes. Accordingly, the fulfilment of requirements such as structural safety, serviceability, traffic safety and
457 durability, must be assured by the designer and the contractor, for all relevant load cases and traffic demands for
458 an indicative design working life of 100 years, according to the current codes. Therefore, quality management
459 strategies for quality control and quality assurance should be employed to reduce or avoid design and construction
460 errors, so the newly constructed bridges are handed over to the owner fulfilling the code's requirements. Such codes
461 are (CEN, 2003, 2005 & 2009), (ISO, 2009b), among others whose the main goal is standardization for quality
462 assurance in bridge design and execution.

463 The Eurocode 0 (CEN, 2005) provides quality management measures aiming at the reduction of errors during the
464 design and execution of structures so that the structures can meet certain reliability levels. For quality management
465 purpose, three design supervision levels and three inspection levels for construction works are proposed according
466 to the reliability classes and consequence classes defined in Eurocode 0 (CEN, 2005) (see Table 6). Similar
467 measures are proposed by (Melchers & Beck, 2018). The (FIB, 2010) proposed as-built documentation that
468 describes the actually constructed structure, including results of the initial inspection and direct input parameters
469 required for maintainability purposes. The recommended structural reliability classes, measured by a target
470 reliability index (β_T), are defined according to the expected consequence (life loss, material damage, functionality
471 losses, among others) of failure of a structure. Hence, three consequence classes are correlated to three reliability
472 classes. The target reliability index stands for the minimum nominal probability of failure that should be assured
473 by the employed design and construction procedures. Nevertheless, Eurocode 0 (CEN, 2005) states that "the actual

474 frequency of failure is significantly dependent upon human errors, which are not considered in partial factor
475 design". Thus, the target reliability index does not necessarily provide an indication of the actual frequency of
476 structural failure since they stand for reliability classes of structures designed and built according to the codes, not
477 necessarily as built.

478 As stated above, the design codes do not take into account human errors in the definition of the threshold value
479 provided for reliability classes since such errors are expected to be eliminated by design supervision and
480 construction inspection, even though this is not always the case. Nonetheless, several attempts in the literature
481 targeting the numerical quantification of human errors impact in structural safety can be found, namely, sensitivity
482 analysis aiming to quantify the impact of different errors in structural safety reduction (Galvão et al. 2019; Nowak
483 & Collins, 2000). Further research, seeking the probabilistic characterization of errors magnitude through
484 probability distribution functions is also available (Haan, 2012; Melchers & Beck, 2018; Qeshmy et al. 2019).
485 Nevertheless, additional investigation is required.

486 On the organization level (Terwel & Jansen, 2015) reported that internal factors regarding interactions between
487 project partners (e.g. agencies, contractors, consultants, designers, owners, reviewers and inspection team) were
488 the ones with the greatest impact on structural safety. Such factors are (i) allocation of responsibility, (ii)
489 coordination, control mechanisms, (iii) communication and collaboration, (iv) safety culture, (v) risk management,
490 among others. External factors such as the economic and political landscape are also important factors to keep in
491 mind. Each organization manages each of these factors according to their internal specification standards and code
492 procedure to tackle human interaction, which is the weakest link in structural design and construction process.

493 **Risk mitigation**

494 The risk analysis is usually followed by a risk evaluation, where the risk of the assessed hazard is compared with
495 acceptance criteria, which sometimes are hard to define and can vary for different industries and societies. The
496 establishment of such acceptance criteria aims to direct proper mitigation actions, to specific hazards, seeking its
497 risk reduction as low as reasonably practicable (ALARP) (Jones-Lee & Aven, 2011). The ALARP concept is
498 directly related to the acceptance criteria; thus, it groups the risk of a hazard into three categories, the critical
499 region, the ALARP region and the acceptable region. A hazard event considered to be present in the critical region
500 cannot be accepted, so it must be reduced at all cost. The ALARP region is characterized by a risk reduction
501 principle targeting the avoidance of a gross disproportion between the risk reduction costs and the obtained risk
502 reduction. Thus, a risk reduction measure must be efficiently employed, so the costs are minimized, and the risk

503 reduction is maximized. (Aven, 2016). For risks within the acceptable region, mitigation is unnecessary, but it is
504 worth mentioning that many of these hazards can lead to unexpected accidents due to their accumulation or long
505 term effect. In this paper, according to the qualitative analysis performed, the critical, ALARP and acceptable
506 regions are identified respectively by the " $Risk \geq 50$ ", " $40 \geq Risk \geq 5$ " and " $Risk \leq 4$ ", respectively, see also
507 Fig. 5 and Fig. 6.

508 As discussed above, the critical zone of the risk matrix usually encompasses risks that must be mitigated at all
509 cost. Consequently, two mitigation actions were suggested by experts for "error due to poor evaluation of the
510 falsework foundation soil properties, and variation of these properties with rainfall", ID 19, see also Fig. 6:

511 **Mitigation Action 1:** Quantification of the soil plastic properties in order to consider further resistance
512 reduction due to rainfall conditions and to better predict the soil maximum bearing capacity.

513 **Mitigation Action 2:** Adoption of a new construction technique (i.e. launching girder) to avoid
514 continuous loading of the soil by the falsework structure.

515 A theoretical curve for the risk reduction and its cost is depicted in Fig. 7. However, for more precise results,
516 a quantitative risk analysis should be performed. With the first mitigation action, the uncertainty concerning the
517 soil properties is decreased; therefore, a risk reduction at a reduced cost can be achieved'. A significant risk
518 reduction can be achieved by the mitigation action two since the adoption of a new construction technique would
519 significantly reduce the error probability of occurrence. However, this mitigation action demands a higher cost
520 than the previous one, since the acquisition or renting cost of a launching girder is considerable.

521 **Conclusion**

522 The design and construction errors are responsible for about 32% of bridges collapse recorded worldwide; hence,
523 they must be carefully addressed. Given the numerous multidisciplinary activities required for the materialization
524 of any idealized engineering structure into its physical equivalent and the human uncertainties in executing such
525 activities, a screening procedure and assessment of the most important sources of errors are demanded. This work
526 provides a framework for such investigation with conclusive outcomes that allow, the design and the construction
527 engineers conceiving the structure to focus their attention on the most relevant errors, and the inspection and the
528 design supervision team to perform enhanced surveillance of the required activities. The framework for the
529 management of human errors risks implement in this research work is summarized according to the following
530 consecutive steps:

- 531 a) An initial screening procedure aiming at the identification of most concerning errors threatening the
532 structural safety of similar structures according to recorded and well-documented failure or collapse
533 cases;
- 534 b) Brainstorming meeting with experts aiming at the identification of errors concerning the on-going project
535 or any other structural system under assessment;
- 536 c) Qualitative risk assessment of the initially identified errors by a carefully selected group of experts;
- 537 d) Prioritization of the errors according to their expected probability of occurrence and consequence leading
538 to the identification of the risk they represent, according to expert's judgement;
- 539 e) Definition of mitigation strategies for errors denoting greater risk and benchmark of their benefits with
540 their costs aiming at the implementation of the most efficient ones;

541 A qualitative categorization of design and construction errors has been performed considering a qualitative risk
542 assessment of such errors by experts through a survey. Different errors risk groups are defined, employing risk
543 matrix and AHP, allowing the prioritization of errors according to their probability of occurrence, consequence
544 and risk. Therefore, a more efficient risk mitigation strategy can be implemented for errors that denote a higher
545 risk for structural safety or construction works, besides overall supervision of the errors that denote lower risks
546 according to standards recommendations. Focusing on the most relevant errors, risk reduction techniques should
547 be effectively implemented, and the structural safety easily assured. Errors concerning geotechnical and falsework
548 malfunctioning, and the system supporting condition changes throughout different construction stages, as well as
549 reinforcement detailing, are highlighted as the errors of highest risk.

550 Furthermore, the impact of three design errors (ID = 4, 13, 17) was numerically assessed in (Galvão et al. 2019)
551 considering a prestressed reinforced concrete overpass. Their impact on structural safety reduction was in
552 accordance with the results obtained with the Analytic Hierarchy Process. Their relative consequence, as ranked
553 in Table 1, was confirmed. Nevertheless, this was not the case for the consequence of two construction errors (ID
554 = 4, 27) also numerically assessed in the same paper.

555 Some design and construction errors go undetected or not reported due to legal implications, but they are
556 usually uncovered after failure. Some errors are detected in existing structures given the structural system
557 underperformance, visible deterioration and deficiencies, non-destructive tests and monitoring systems, but still,
558 many of them go undetected. Thus, the assessment of existing structures should employ strategies for the

559 identification of design and construction errors that are likely to lead to the underperformance of the structural
560 system, service life reduction or even structural collapse.

561 **Data availability statements**

562 Some or all data, models, or code generated or used during the study are proprietary or confidential in nature and
563 may only be provided with restrictions. That is **1.** Bridge failure database (IABSE's Task Group 1.5 proprietary).
564 **2.** Matlab script implementing the Analytic Hierarchy Process (authors proprietary). **3.** Information collected with
565 the survey (authors proprietary). Requests for the first item must be directed to IABSE. The last two items are
566 meant to be kept confidential for further research work, publications and surveyed experts data protection.

567 **Acknowledgements**

568 This research was developed at the University of Minho in close cooperation with the following entities: Adão da
569 Fonseca, COST Action TU 1406, GEG, HDP, IABSE, Portuguese Infrastructures, Mota Engil and Soares da Costa.
570 This work was partly financed by: (i) FEDER funds through the Competitvity Factors Operational Programme
571 (COMPETE) and by national funds through the Foundation for Science and Technology (FCT) within the scope
572 of project POCI 01 0145 FEDER 007633; (ii) national funds through FCT - Foundation for Science and
573 Technology, under grant agreement "PD/BD/143003/2018" attributed to the 1st author; and (iii) FCT / MCTES
574 through national funds (PIDDAC) under the R&D Unit Institute for Sustainability and Innovation in Structural
575 Engineering (ISISE), under reference UIDB / 04029/2020.

576 **References**

- 577 Aven, T. (2016). Risk assessment and risk management: Review of recent advances on their foundation. *Eur. J.*
578 *Oper. Res.*, 253(1), 1–13. <https://doi.org/10.1016/j.ejor.2015.12.023>
- 579 Ayub, M. (2019). *Investigation of March 15, 2018 Pedestrian Bridge Collapse at Florida International Univesity,*
580 *Miami, Florida.* Washington, D.C.
- 581 Bridge Design Engineering. (2018). Report published on fatal Colombian bridge collapse. Retrieved September
582 18, 2020, from <https://www.bridgeweb.com/Report-published-on-fatal-Colombian-bridge-collapse/4659>
- 583 Canisius, T. D. G., Barker, J. B., Diamantidis, D., Ellingwood, B. R., Faber, M., Holicky, M., ... Vrouwenvelder,
584 T. (2011). *Structural Robustness Design for Practising Engineers. COST Action TU0601: Robustness of*
585 *Structures.*

- 586 Cavaco, E. S. (2013). *PhD Thesis: Robustness of corroded reinforced concrete structures*. University of Lisbon.
- 587 Chen, T. T. (2017). Factors in Bridge Failure, Inspection, and Maintenance. *J. Perform. Constr. Facil.*, *31*(5),
588 04017070. [https://doi.org/10.1061/\(ASCE\)CF.1943-5509.0001042](https://doi.org/10.1061/(ASCE)CF.1943-5509.0001042)
- 589 Deng, L., Wang, W., & Yu, Y. (2016). State-of-The-Art Review on the Causes and Mechanisms of Bridge
590 Collapse. *J. Perform. Constr. Facil.*, *30*(2), 04015005. [https://doi.org/10.1061/\(ASCE\)CF.1943-5509.0000731](https://doi.org/10.1061/(ASCE)CF.1943-5509.0000731)
591
- 592 engineering .com. (2019). How Machine Learning is Improving Construction. Retrieved August 10, 2020, from
593 [https://www.engineering.com/BIM/ArticleID/19317/How-Machine-Learning-is-Improving-](https://www.engineering.com/BIM/ArticleID/19317/How-Machine-Learning-is-Improving-Construction.aspx)
594 [Construction.aspx](https://www.engineering.com/BIM/ArticleID/19317/How-Machine-Learning-is-Improving-Construction.aspx)
- 595 Epaarachchi, D. C., & Stewart, M. G. (2004). Human Error and Reliability of Multistory Reinforced-Concrete
596 Building Construction. *J. Perform. Constr. Facil.*, *18*(1), 12–20. [https://doi.org/10.1061/\(ASCE\)0887-3828\(2004\)18:1\(12\)](https://doi.org/10.1061/(ASCE)0887-3828(2004)18:1(12))
597
- 598 European Committee for Standardization (CEN). (2005). *EN 1990, Eurocode 0: Basis of structural design*.
599 Brussels, Belgium.
- 600 European Committee for Standardization (CEN). (2003). *EN 1991-2, Eurocode 1: Actions on structures - Part 2:
601 Traffic loads on bridges*. Brussels, Belgium.
- 602 European Committee for Standardization (CEN). (2005). *EN 1992-2: Eurocode 2: Design of concrete structures
603 - Part 2: Concrete bridges - Design and detailing rules*. Brussels, Belgium.
- 604 European Committee for Standardization (CEN). (2009). *EN 13670, Execution of concrete structures*. Brussels,
605 Belgium. Faber, M. H. J. (2008). *Risk Assessment in Engineering: Principles, System Representation & Risk
606 Criteria*.
- 607 Fröderberg, M. (2014). *The human factor in structural engineering : a source of uncertainty and reduced
608 structural safety*. Lund University.
- 609 Fröderberg, M. (2015). Conceptual Design Strategy: Appraisal of Practitioner Approaches. *Struct. Eng. Int.*,
610 *25*(2), 151–158. <https://doi.org/10.2749/101686614x14043795570615>
- 611 Galvão, N., Campos e Matos, J., Oliveira, D., & Santos, C. (2019). Assessment of roadway bridges damaged by

- 612 human errors using risk indicators and robustness index. In *IABSE Symposium, Guimaraes 2019: Towards*
613 *a Resilient Built Environment Risk and Asset Management - Report* (pp. 236–243). Guimarães, Portugal.
- 614 Goepel, K. D. (2013). Implementing the Analytic Hierarchy Process as a Standard Method for Multi-Criteria
615 Decision Making In Corporate Enterprises – A New AHP Excel Template with Multiple Inputs. In
616 *Proceedings of the International Symposium on the Analytic Hierarchy Process* (pp. 1–10). Kuala Lumpur,
617 Malaysia. <https://doi.org/10.13033/isahp.y2013.047>. The template can be downloaded from
618 <http://bpmsg.com>.
- 619 Goepel, K. D. (2018). Implementation of an Online software tool for the Analytic Hierarchy Process (AHP-OS).
620 *Int. J. Anal. Hierarchy Process*, 10(3), 469–487. <https://doi.org/10.13033/isahp.y2018.029>
- 621 Haan, J. (2012). *Msc Thesis: Human Error in Structural Engineering: The design of a Human Reliability*
622 *Assessment method for Structural Engineering*. Delft University.
- 623 Imhof, D. (2004). *PhD Thesis: Risk Assessment of Existing Bridge Structures*. University of Cambridge.
- 624 International Federation for Structural Concrete (FIB). (2010). *Model Code for Concrete Structures*. Lausanne,
625 Switzerland: Ernst&Sohn.
- 626 International Organization for Standardization (ISO). (2009a). *IEC/ISO 31010, Risk management - Risk*
627 *assessment techniques* (1.0). Geneva, Switzerland: International Electrotechnical Commission (IEC).
- 628 International Organization for Standardization (ISO). (2009b). *ISO 22966:2009 - Execution of concrete structures*.
629 Geneva, Switzerland.
- 630 International Organization for Standardization (ISO). (2015). *ISO 2394, General Principles on Reliability for*
631 *Structures*. Switzerland.
- 632 Johnson, P. A., Clopper, P. E., Zevenbergen, L. W., & Lagasse, P. F. (2015). Quantifying Uncertainty and
633 Reliability in Bridge Scour Estimations. *J. Hydraul. Eng.*, 141(7), 04015013.
634 [https://doi.org/10.1061/\(asce\)hy.1943-7900.0001017](https://doi.org/10.1061/(asce)hy.1943-7900.0001017)
- 635 Joint Committee on Structural Safety (JCSS). (2001). *Probabilistic Model Code - Part 1: Basis of design*.
- 636 Jones-Lee, M., & Aven, T. (2011). ALARP - What does it really mean? *Reliab. Eng. Syst. Saf.*, 96(8), 877–882.
637 <https://doi.org/10.1016/j.ress.2011.02.006>

- 638 Kifokeris, D., & Xenidis, Y. (2019). Risk source-based constructability appraisal using supervised machine
639 learning. *Autom. Constr.*, *104*, 341–359. <https://doi.org/10.1016/j.autcon.2019.04.012>
- 640 Kifokeris, D., e Matos, J. A. C., Xenidis, Y., & Bragança, L. (2018). Bridge quality appraisal methodology:
641 Application in a reinforced concrete overpass roadway bridge. *J. Infrastruct Syst.*, *24*(4), 04018034.
642 [https://doi.org/10.1061/\(ASCE\)IS.1943-555X.0000455](https://doi.org/10.1061/(ASCE)IS.1943-555X.0000455)
- 643 Manfreda, S., Link, O., & Pizarro, A. (2018). A theoretically derived probability distribution of scour. *Water*,
644 *10*(11). <https://doi.org/10.3390/w10111520>
- 645 Maskin entreprenoren. (2020). AI to prevent fatalities | Machine contractor. Retrieved September 27, 2020, from
646 <https://maskinentreprenoren.se/ai-ska-hindra-dodliga-olyckor/>
- 647 Melchers, R., & Beck, A. T. (2018). *Structural Reliability Analysis and Prediction*. (3rd Editio). New York.: John
648 Wiley & Sons Ltd.,.
- 649 Morgese, M., Ansari, F., Domaneschi, M., & Cimellaro, G. P. (2020). Post-collapse analysis of Morandi's
650 Polcevera viaduct in Genoa Italy. *J. Civ. Struct. Heal. Monit.*, *10*(1), 69–85.
651 <https://doi.org/10.1007/s13349-019-00370-7>
- 652 Nowak, A. S., & Collins, K. R. (2000). *Reliability of structures*. (McGraw-Hill, Ed.) (2nd ed.). Thomas Casson.
- 653 NTSB. (2018). Miami bridge that collapsed and killed 6 had design errors. Retrieved September 6, 2020, from
654 <https://eu.usatoday.com/story/news/2018/11/15/ntsb-miami-bridge-collapse-design-errors/2012020002/>
- 655 Pujol, S., Kreger, M. E., Monical, J. D., & Schultz, A. E. (2019). Investigation of the Collapse of the Chirajara.
656 *Concr. Int.*, *41*(6), 29–37.
- 657 Qeshmy, D., Makdisi, J., Ribeiro da Silva, E., & Angelis, J. (2019). Managing Human Errors: Augmented Reality
658 systems as a tool in the quality journey. *Procedia Manuf.*, *28*, 24–30.
659 <https://doi.org/10.1016/J.PROMFG.2018.12.005>
- 660 Rausand, M. (2011). *Risk assessment: Theory, Methods, and Applications*. New Jersey: John Wiley & Sons.
661 Retrieved from NS -
- 662 Saaty, T. L., & Vargas, L. G. (2013). *Decision Making with the Analytic Network Process* (2nd ed.). Boston, MA,
663 USA: Springer. <https://doi.org/10.1007/978-1-4614-7279-7>

- 664 Scheer, J. (2010). *Failed Bridges - Case Studies, Causes and Consequences*. Hannover: Ernst&Sohn.
665 <https://doi.org/10.1002/9783433600634>
- 666 Starossek, U., & Haberland, M. (2010). Disproportionate Collapse: Terminology and Procedures. *J. Perform.*
667 *Constr. Facil.*, 24(6), 519–528. [https://doi.org/10.1061/\(asce\)cf.1943-5509.0000138](https://doi.org/10.1061/(asce)cf.1943-5509.0000138)
- 668 Stewart, M. G., & Melchers, R. E. (1988). Simulation of human error in a design loading task. *Struct. Saf.*, 5(4),
669 285–297. [https://doi.org/10.1016/0167-4730\(88\)90029-X](https://doi.org/10.1016/0167-4730(88)90029-X)
- 670 Sykora, M., Diamantidis, D., Holicky, M., & Jung, K. (2017). Target reliability for existing structures considering
671 economic and societal aspects. *Struct. Infrastruct. Eng.*, 13(1), 181–194.
672 <https://doi.org/10.1080/15732479.2016.1198394>
- 673 Syrkov, A. (2017). Review of bridge collapses worldwide 1966 - 2018. In *IABSE Workshop: Ignorance,*
674 *uncertainty and human errors in structural engineering*. Helsinki, Finland.
- 675 Terwel, K. C., & Jansen, S. J. T. (2015). Critical Factors for Structural Safety in the Design and Construction
676 Phase. *J. Perform. Constr. Facil.*, 29(3), 04014068. [https://doi.org/10.1061/\(asce\)cf.1943-5509.0000560](https://doi.org/10.1061/(asce)cf.1943-5509.0000560)
- 677 The New York Times. (2018). Genoa Bridge Collapse: The Road to Tragedy. Retrieved September 6, 2020, from
678 <https://www.nytimes.com/interactive/2018/09/06/world/europe/genoa-italy-bridge.html>
- 679 Thompson, P. D., Patidar, V., Labi, S., Sinha, K., Hyman, W. A., & Shirolé, A. (2006). Multi-objective
680 optimization for bridge management. In *Proceedings of the 3rd International Conference on Bridge*
681 *Maintenance, Safety and Management - Bridge Maintenance, Safety, Management, Life-Cycle Performance*
682 *and Cost* (pp. 735–736). Porto, Portugal.
- 683 Tylek, I., Kuchta, K., & Rawska-Skotniczny, A. (2017). Human Errors in the Design and Execution of Steel
684 Structures—A Case Study. *Struct. Eng. Int.*, 27(3), 370–379.
685 <https://doi.org/10.2749/101686617X14881937385287>
- 686 Zambon, I., Vidovic, A., Strauss, A., Matos, J. (2019). Use of chloride ingress model for condition assessment in
687 bridge management. *J. Croat. Assoc. Civ. Eng.*, 71(5), 359–373. <https://doi.org/10.14256/JCE.2411.2018>

Table 1 – List of design errors identified and analysed

Errors Cluster	ID	List of Errors	Rankings	
			PO	CO
Structural Analysis and Design Errors	1	Error due to a non-conservative arrangement between design and load regulations with different backgrounds, leading to a less reliable structure	16	17
	2	Errors in regulations interpretation	9	20
	3	Error in live loads quantification due to lack of data	13	14
	4	Error in dead load quantification	20	1
	5	Error in the definition of the most significant load combinations	11	7
	6	Error in defining the gravity centre for highly compressed elements, or in defining load eccentricity	18	11
	7	Error in defining a cross-section shear centre (torsion effects)	7	18
	8	Error in the quantification of the effects of deck deformation due to creep, shrinkage and temperature variation, in columns (second-order effects)	1	16
	9	Error in defining the buckling length of an element	12	10
	10	Error in defining/describing the location of prestressing tendons	15	8
	11	Error in the decompression limit state calculation	14	19
	12	Error in defining the prestressing hyperstatic effects	3	15
	13	Error in defining the soil-structure interaction (boundary conditions and differential settlements)	2	12
	14	Error due to lack of consideration of different support conditions that a bridge or an element will be subjected through the construction process	5	2
	15	Error in modelling the connections between structural elements (e.g. deck, beams and columns)	8	5
Detailing Errors	16	Error due to the lack of consistency between the design assumptions and the detailing rules	4	9
	17	Error in reinforcement cross-section area	17	3
	18	Error in reinforcement spacing (flexural and shear reinforcement)	10	4
	19	Error in concrete and reinforcement classes indication	19	6
	20	Error in defining the quota of implantation	6	13

Table 2 – List of construction errors identified and analysed

Errors Cluster	ID	List of Errors	Rankings	
			PO	CO
Material Quality Control Errors	Concrete	1 Errors leading to alkali-aggregate reaction	19	15
		2 Error in the quantification of cement hydration heat	18	22
		3 Error in the evaluation of aggregates humidity	13	28
		4 Error due to poor concrete workmanship leading to concrete with characteristics and properties different from the requested	22	13
	Reinforcement	5 Errors leading to reinforcement corrosion	10	25
		6 Error using a wrong reinforcement class especially when different reinforcement classes are also used in construction	29	23
		7 Error in the production of reinforcement cross-section area	26	14
Execution Errors	Generic Errors	8 Error due to wrong positioning of supports	15	12
		9 Error due to expansion joints deficiency and wrongly positioned	3	19
		10 Error due to wrong interpretation of the design project	21	8
		11 Error in topographic implantation	14	16
		12 Error due to wrong concrete vibration	20	27
		13 Error in the reinforcement covering	2	18
		14 Error in the longitudinal shape due to shrinkage and creep effects not correctly computed in the design phase	9	26
		15 Error due to consideration of support conditions different from those defined in the design phase	23	24
	Falsework Execution Errors	16 Error due to the establishment of wrong final boundary conditions	25	20
		17 Error due to wrong evaluation of the foundation soil properties	5	4
		18 Error due to geometric imperfections (inclination and cross-section imperfection)	11	29
		19 Error due to poor evaluation of the falsework foundation soil properties, and variation of these properties after rainfall	1	3
		20 Error due to poor preparation of the falsework foundation using gravel material and/or poor positioning of the timber elements that support the falsework	8	10
		21 Error due to deficiency in the continuous falsework bracing, leading to global instability	4	1
		22 Error due to a deficient maintenance plan leading to poor falsework material quality	12	7
		23 Error in the falsework clamping elements (connectors and couplers)	6	6
		24 Error in movable falsework due to non-controlled hyperstaticity reduction to perform his movement	16	2
		25 Error in the assessment of the formwork and falsework deformability properties	7	17
Prestressing Errors	26 Error due to wrong positioning of formwork ties	17	21	
	27 Error due to insufficient prestressing	28	5	
	28 Error due to over loss of prestressing	24	11	
	29 Error due to insufficient curing of concrete subjected to prestressing forces leading to a deficient bond between the concrete and the prestressed cables	27	9	

692

Table 3 – List of additional design errors collected within the survey

Errors Cluster		List of Errors
Structural Analysis and Design Errors		Error due to low design experience
		Error due to accelerated design programmes to meet deadlines and design budgets
		Error due to incorrect application and understanding of partial prestressing
		Error due to incorrect use of structural analysis software
		Errors of data entry in structural software's (e.g. material strength, boundary and nodal constraints, self-weight, elasticity modulus. etc.)
		Error due to non-validation of automatic computation of complex numerical models with simpler models
		Error due to hydrostatic effects negligence in the structural analysis
		Error due to the project non-verification by authorized and qualified design reviewers
Detailing Errors		Lack of experience with good detailing practices (mainly in steel structures)
		Error due to drawings misinterpretation due to lack of experience and awareness
		Error due to the use of general details drawings from existing projects
		Error due to lack of coherence between shear reinforcement detailing and different details

693

694

Table 4 – List of additional construction errors collected within the survey

Errors Cluster		List of Errors	
Material Quality Control Errors	Concrete	Error due to non-attendance of quality control expert inspectors to the construction site	
		Error due to lack of protective measures in very high and low-temperature work sites	
	Reinforcement	Error due to non-attendance of quality control expert inspectors to the construction site	
		Error due non-conformity of steel reinforcement bars with standards	
Execution Errors	Generic Errors	Clashing of reinforcement (particularly for precast elements)	
		Error in the execution of the abutment's embankments	
		Error due to deficiency in the execution of the approach slabs	
		Errors or deficiencies caused by interrupted concreting because of equipment malfunctioning or delays of the concreting mixer trucks	
		Error due to non-controlled concreting of mass concrete elements leading to high temperatures in the concrete core (spread foot of abutments and piers, pile cap, among others)	
	Falsework Execution Errors		Errors due to the inexistence of checklist or check procedures for execution quality control
			Errors caused by changes in the assembly technique and material concerning the execution project
			Errors due to the usage of uncertified materials
		Errors caused by the absence of the rainwater drainage system or any other protective measure	

695

696

697

698

699

Table 5 – Top five design and construction errors with the highest risk

Design Errors	Construction Errors
Error due to lack of consideration of different support conditions that a bridge or an element will be subjected through the construction process; (ID 14)	Error due to deficiency in the continuous falsework bracing leading to global instability (ID 21)
Error in reinforcement cross-section area detailing; (ID 17)	Error due to poor evaluation of the falsework foundation soil properties, and variation of these properties after rainfall (ID 19)
Error due to lack of consistency between the design assumptions and the detailing rules; (ID 16)	Error in movable falseworks due to non-controlled hyperstaticity reduction needed to perform his movement (ID 24)
Error in the definition of the soil-structure interaction (e.g. boundary conditions and differential settlements); (ID 13)	Error due to wrong evaluation of the foundation soil properties (ID 17)
Error in modelling the connections between structural elements (e.g. deck, beams and columns); (ID 15)	Error in the falsework clamping elements (connectors and couplers) (ID 23)

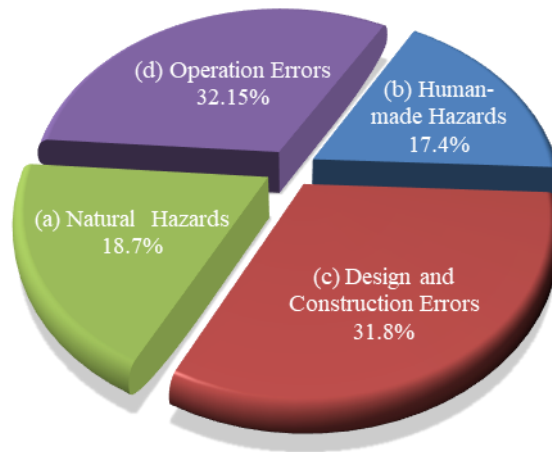
700

701 Table 6 – Design supervision and construction works inspection levels according to Eurocode 0 (CEN, 2005)

Reliability Class (RC)*	Examples of buildings and civil engineering works (ISO, 2015)	Design supervision levels	Inspection Levels
RC3 ($\beta_T = 4.3$)	Major bridges and public buildings where consequences of failure are high (e.g. fewer than 500 fatalities)	Third-party checking: Checking performed by an organizational different from that which has prepared the design	Third-party inspection
RC 2 ($\beta_T = 3.8$)	Typical bridges, residential, office buildings and public buildings where consequences of failure are medium (e.g. fewer than 50 fatalities)	Checking by different persons than those originally responsible and in accordance with the procedure of the organization	Inspection in accordance with the procedures of the organisation
RC 1 ($\beta_T = 3.3$)	Agricultural buildings where people do not normally enter (e.g. storage buildings), greenhouse	Self-checking: Checking performed by the person who has prepared the design	Self-inspection

702

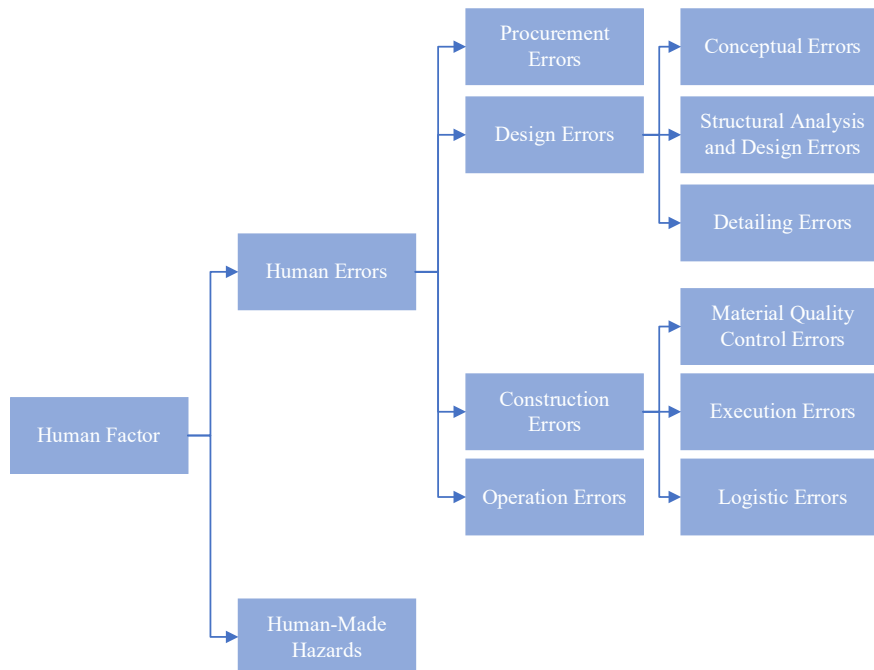
*Target reliability levels established for ultimate limit states for 50 years reference period.



703

704

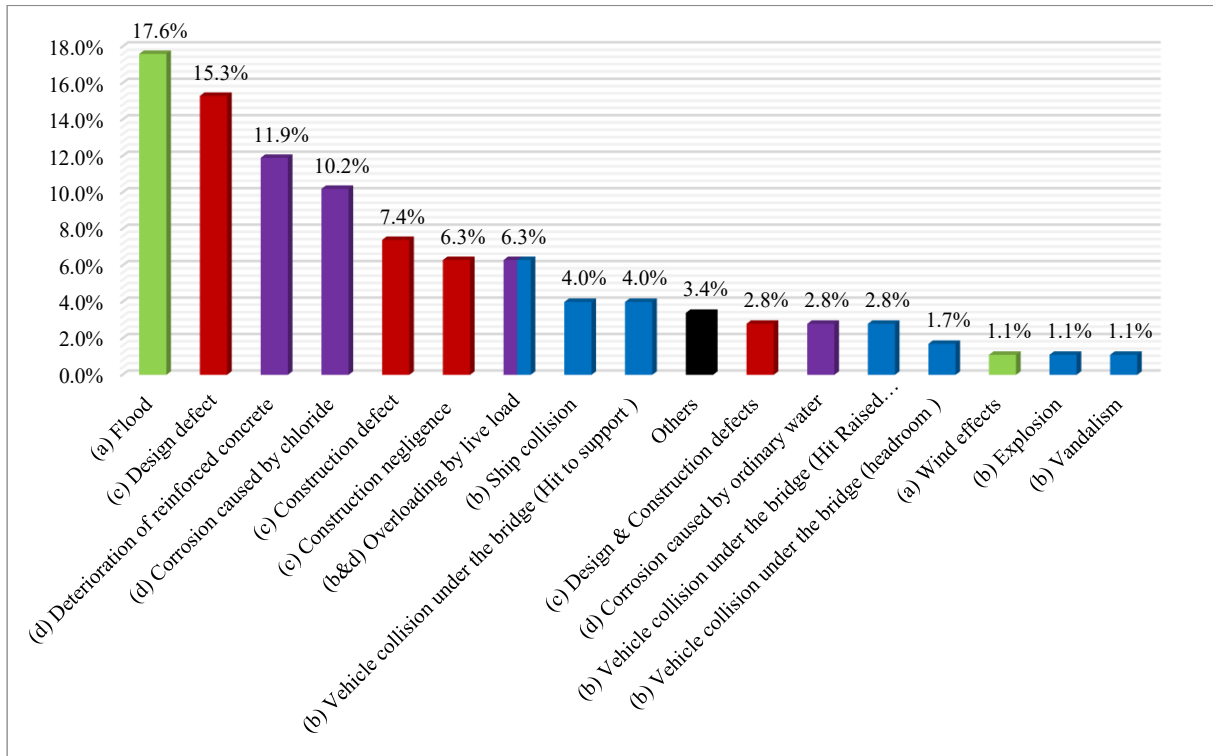
Fig. 1 – Main causes of failure of reinforced concrete bridges (Syrkov, 2017)



705

706

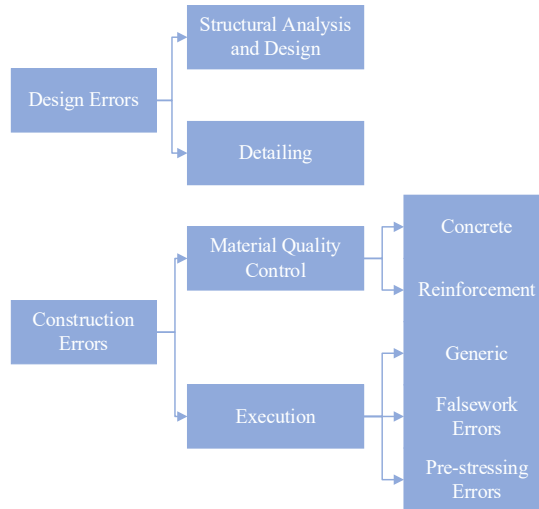
Fig. 2 – Human error clusters



707

708

Fig. 3 – Specific causes of failure for reinforced concrete bridges



709

710

Fig. 4 – Design and construction error clusters

Risk = PO x CO		Impact or Consequences (CO)					
		Very Low	Low	Average	High	Very High	
		1	2	5	10	20	
Probability of Occurrence (PO)	Very High	5					
	High	4					
	Average	3			8, 12, 13, 16, 20	14	
	Low	2		11	2, 3, 9, 5, 10, 18	17	
	Very Low	1			1, 6, 19	4	

711

712

Fig. 5 - Risk matrix of design errors

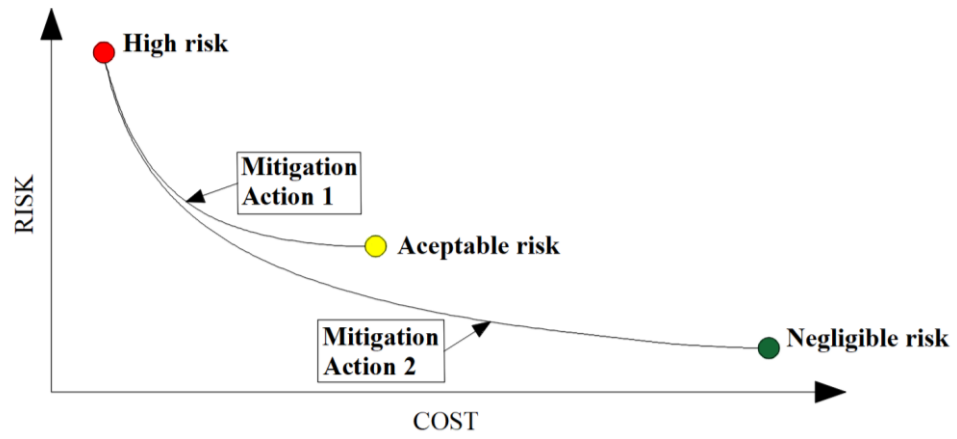
Risk = PO x CO		Impact or Consequences (CO)					
		Very Low	Low	Average	High	Very High	
		1	2	5	10	20	
Probability of Occurrence (PO)	Very High	5					
	High	4					
	Average	3		9	13		19
	Low	2		14, 5, 18, 3, 12, 15, 16	25, 11, 1, 8, 4, 28, 7, 29, 20, 22, 10	17, 23	
	Very Low	1		6	27, 24		

713

714

Fig. 6 - Risk matrix of construction errors

715



716

717

718

719

720

Fig. 7 – Risk reduction due to the mitigation actions